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# **Notch Sensitivity and Damage Tolerance of Composite Sandwich Structures**

**Dan Adams**

**Marcus Stanfield**

**Brad Kuramoto**

**Martin Raming**

**University of Utah**

**2018 Technical Review**



# FAA Sponsored Project Information

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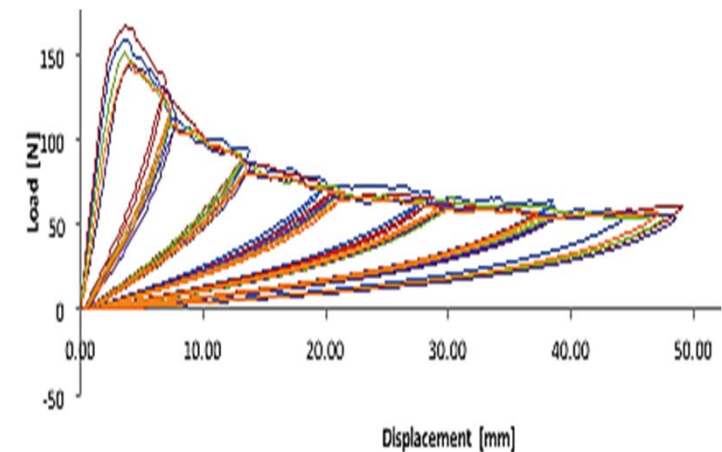
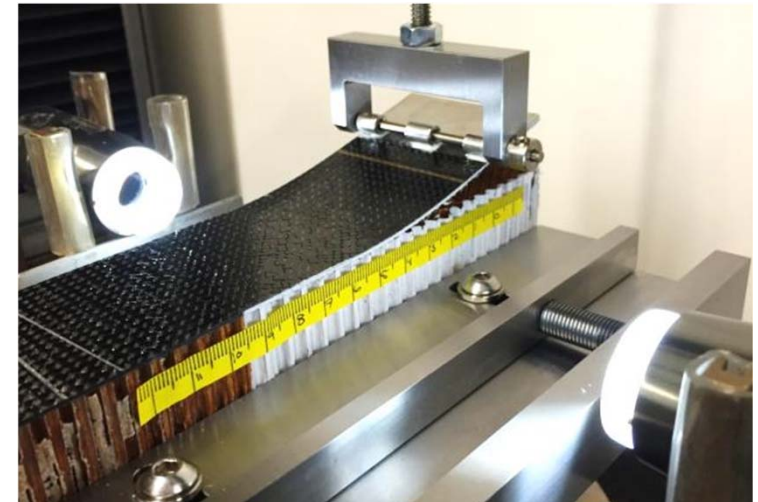
- **Principal Investigators:**
  - Dr. Dan Adams**
  - Dr. Mike Czabaj**
- **Graduate Student Researchers:**
  - Marcus Stanfield**
  - Brad Kuramoto**
  - Martin Raming**
- **FAA Technical Monitor:**
  - Zhi-Ming Chen**
- **Primary Collaborators:**
  - Materials Sciences Corporation**
  - Boeing (Charles Park)**
  - ASTM D30 (Composites)**

# Status Update:

## Mode I Sandwich Fracture Mechanics Test Method

### Standardization of Single Cantilever Beam (SCB) Test

- Second subcommittee ballot in ASTM subcommittee D30.09
- Negative votes discussed at recent ASTM D30 meeting and follow-on teleconference
  - Mode mixity: “Mode I dominant”
  - Acceptable disbond location: within top one-fourth of core
- Additional details to be included in CMH-17
- Concurrent D30 subcommittee & main committee ballot in June

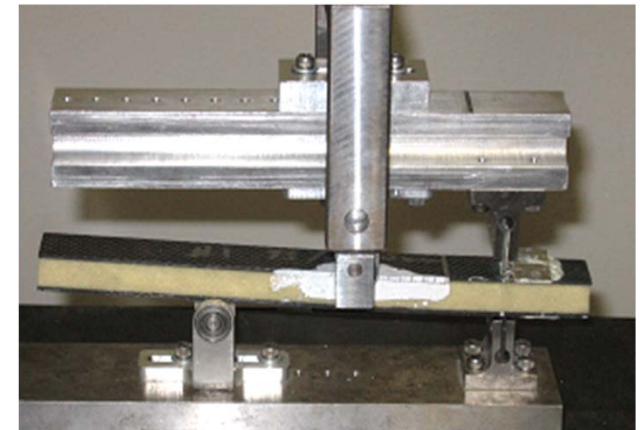
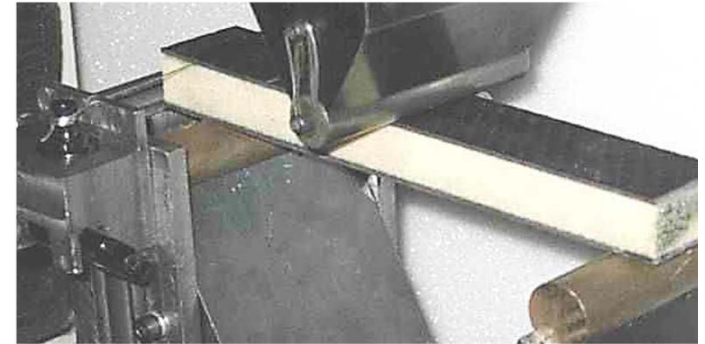


# *Status Update:*

## **Additional Sandwich Disbond Related Activities**

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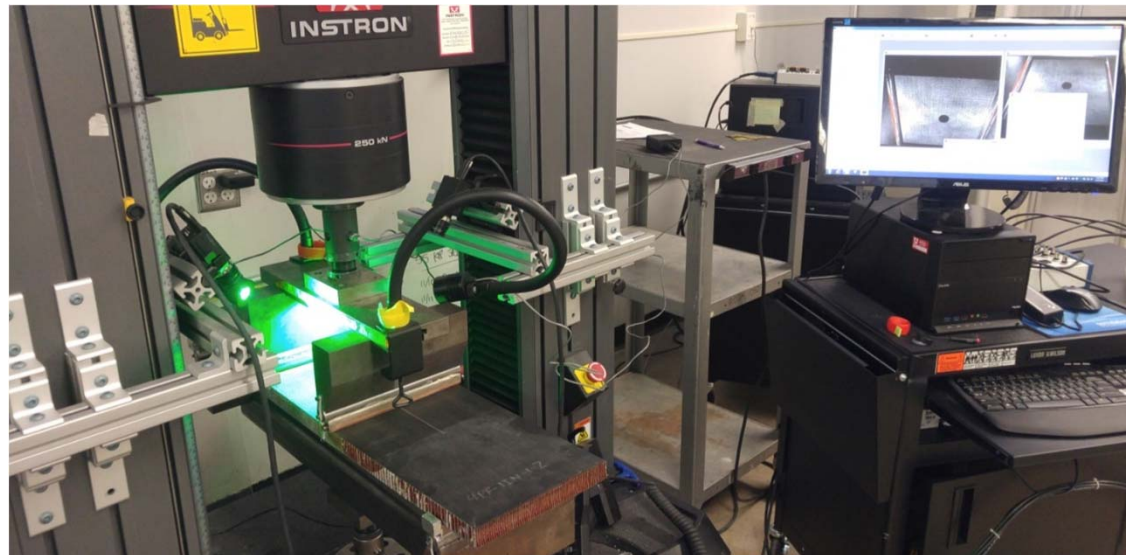
- **SCB fatigue test method development**
- **Further Mixed-Mode & Mode II sandwich disbond test method development**
- **Follow-on U.S. led building block exercise**
  - **Core, facesheet, and film adhesives obtained**
  - **Follow-on coupon and sub-element level testing**
  - **Analysis round-robin**
- **New content for upcoming revision of CMH-17 Handbook**



# *Status Update:*

## Sandwich Damage Tolerance

- **Draft standard of Sandwich composite Compression After Impact (SCAI) completed**
  - Balloted Spring 2018 ASTM D30 meeting
  - Updates to address negative votes in work
- **Draft practice of 4-Point Flexure After Impact (4-FAI) in progress**



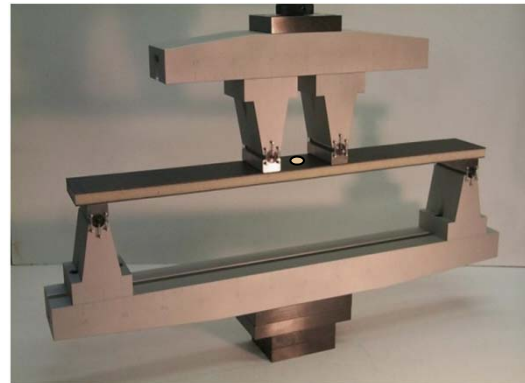
# Research Objectives:

## Notch Sensitivity of Sandwich Composites

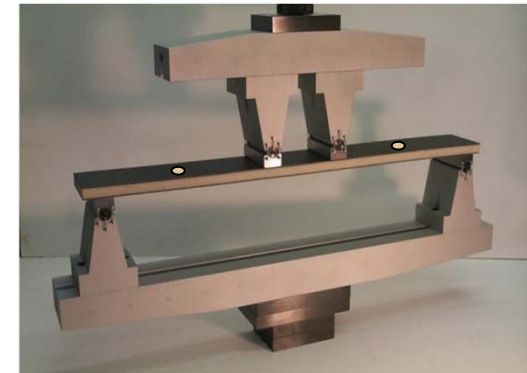
- Initial development of notched test methods & associated analysis methodologies for composite sandwich panels
- Documentation of notched testing and analysis protocols in Composites Materials Handbook (CMH-17)
- Explore development of new ASTM standards for notch sensitivity of sandwich composites



**Sandwich Open Hole  
Compression**



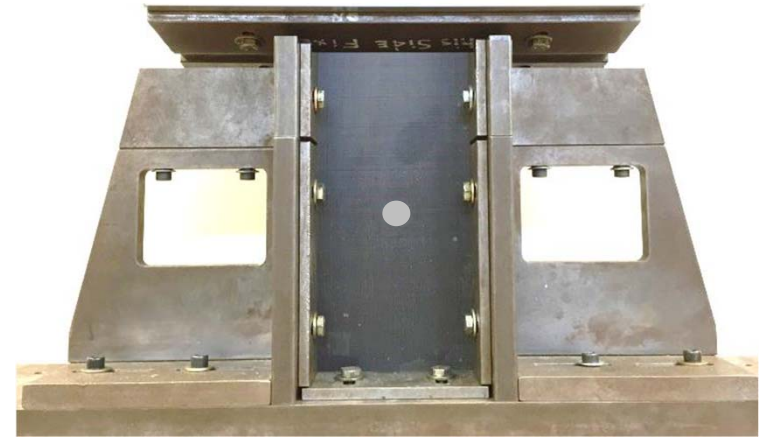
**Sandwich Open Hole  
Flexure**



**Notched Core Shear  
Beam Flexure**

# Testing Considerations: Sandwich Open-Hole Compression

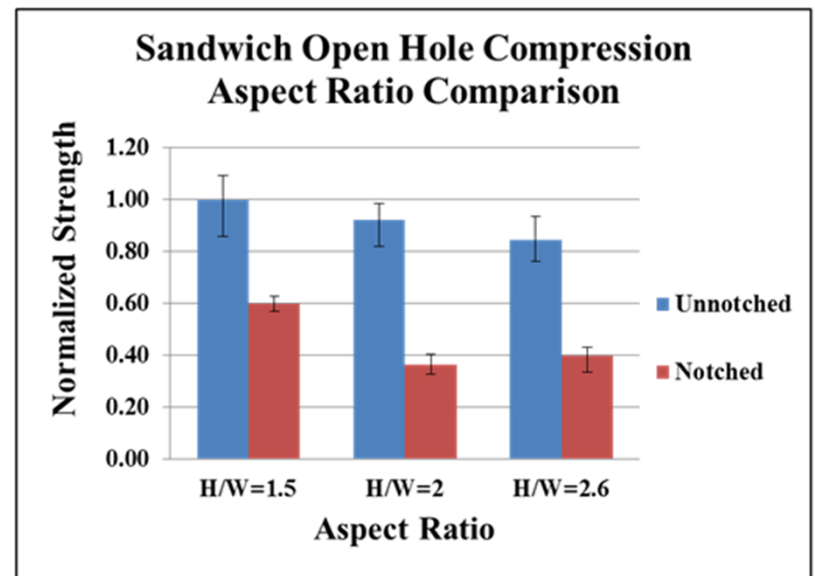
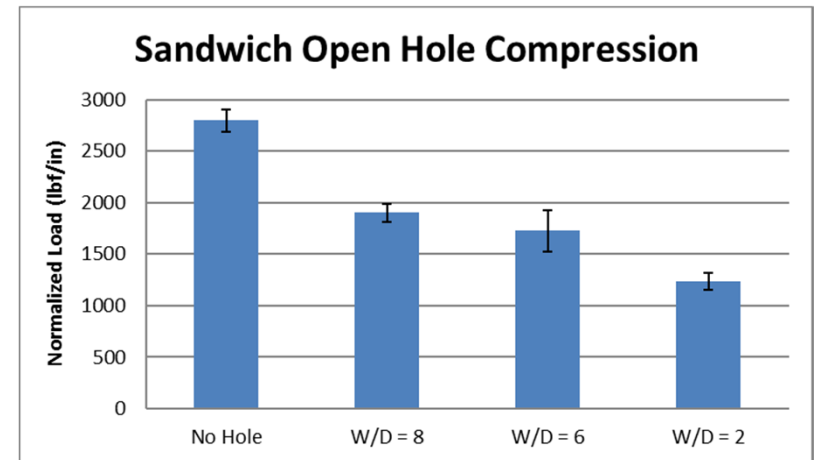
- **Test fixture/Specimen support**
  - End supports
    - Clamping top and bottom
    - Potting
  - Side supports
    - Knife edge
- **Specimen size**
  - Separation of central hole and boundary effects
  - Production of acceptable strength reductions
- **Strain measurement**
- **Specimen alignment**



Open hole compression fixture  
for monolithic composites

# Sandwich Open-Hole Compression: Determination of Sizing Guidelines

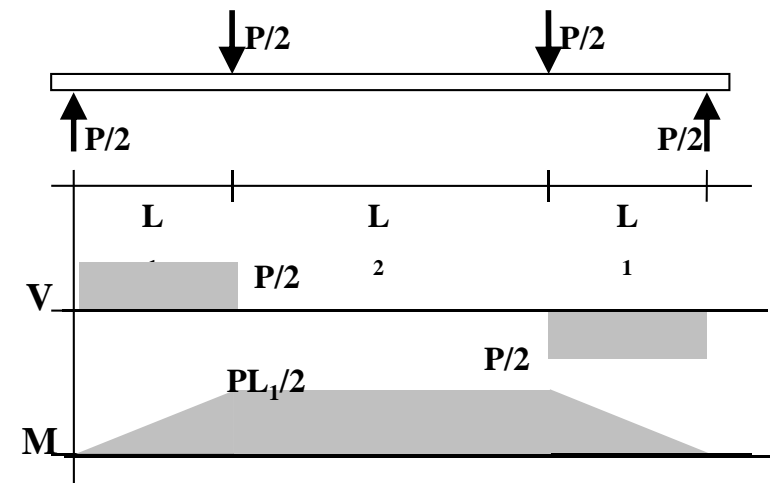
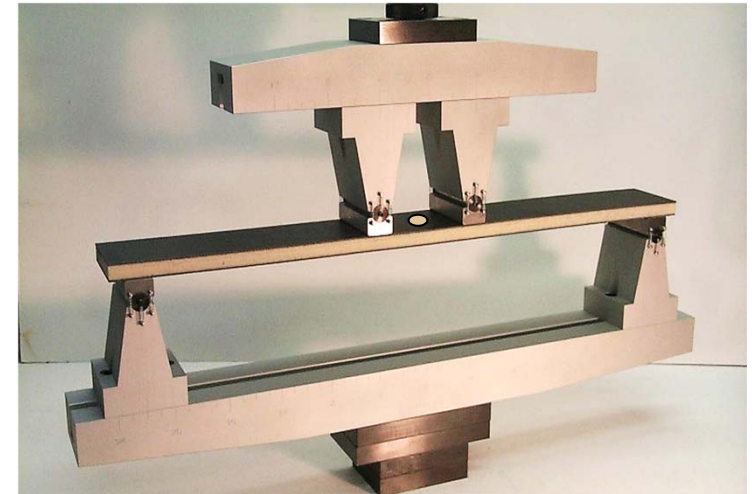
- Hole diameter (W/D)
  - Legacy:  $W/D = 6$
  - Acceptable strength reduction
  - Minimal finite width effects
- Aspect ratio (H/W)
  - $H/W = 2$
  - Acceptable strength reduction
- Standard configuration
  - Width: 4 in.
  - Height: 8 in.
  - Hole Diameter: 0.67 in.





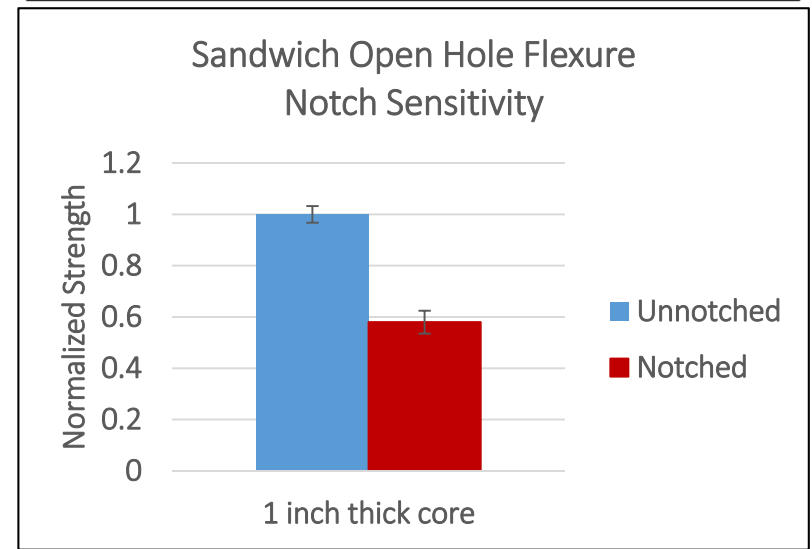
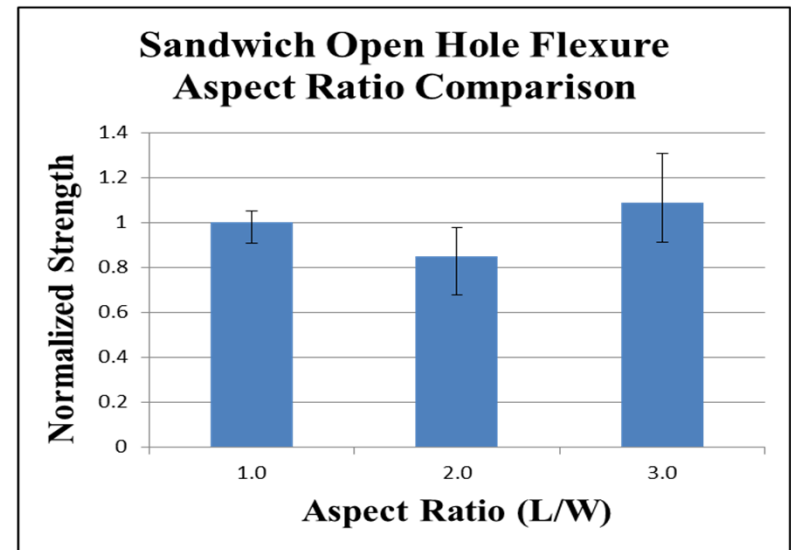
# Testing Considerations: Sandwich Open-Hole Flexure Test

- **Test fixture/Specimen support**
  - Inner span
    - Separation of notch and loading boundary effects
  - Outer span
    - Develop sufficient bending moment
    - Ensure failure in inner span
- **Required specimen width**
  - Separation of central hole and specimen edges
  - Production of acceptable strength reduction



# Sandwich Open-Hole Flexure Test: Determination of Sizing Guidelines

- **Current configuration**
  - Specimen width  $W = 3$  in.
  - Hole diameter  $D = 0.5$  in.
  - Inner span  $L = 4$  in.
  - Outer span sized to ensure inner span failure
- **No inner span aspect ratio sensitivity ( $L/W$ )**
  - Inner span can be increased for measurement purposes



# Third Loading Configuration: Core Damage and Notch Effects

- Effects of core notch or core damaged on material response
  - Notched core shear
    - Circular centered thru holes
    - Beam flexure
  - Sandwich disbond after core crush
    - Quasi-static indentation
    - Multiple crush geometries
    - SCB Mode I fracture testing



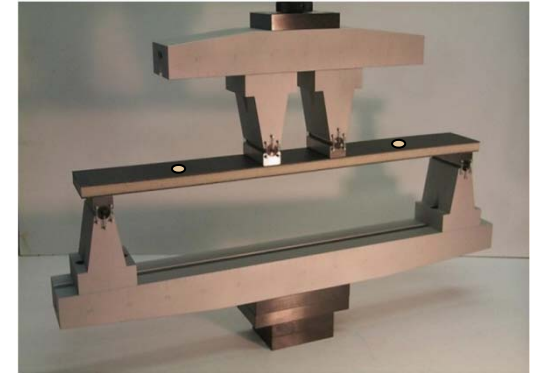
Notched Core Shear by Beam Flexure



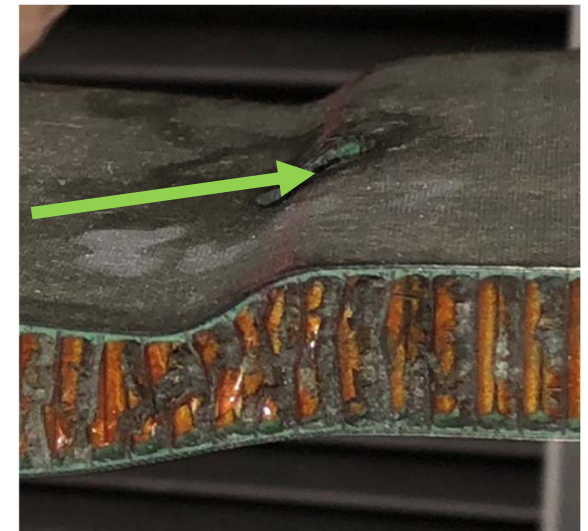
Disbond after Core Crush

# Testing Considerations: Notched Core Shear by Beam Flexure

- Investigating notch effects in Nomex honeycomb core
- Three-point flexure loading
- Sandwich configurations:
  - $W = 3$  in.  $L = 8$  in.  $C = 0.5$  in.
  - 3 pcf 1/8 in. cell Nomex
  - Notched & Unnotched
- Through hole, 0.5 in. dia ( $W/D=6$ )
- Sized to ensure core shear failure (ASTM C393)
- L and W core directions tested



Notched Core Shear  
Beam Flexure

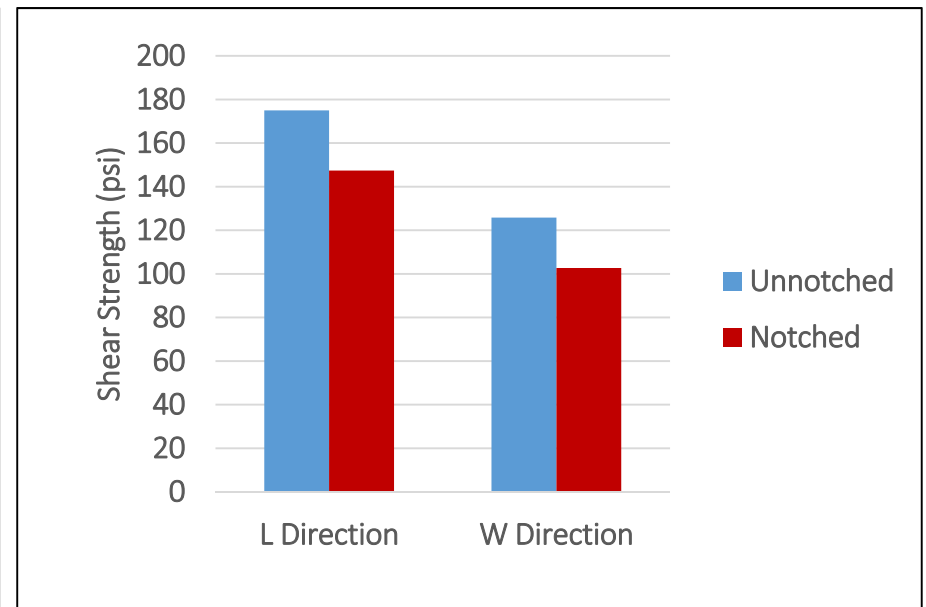
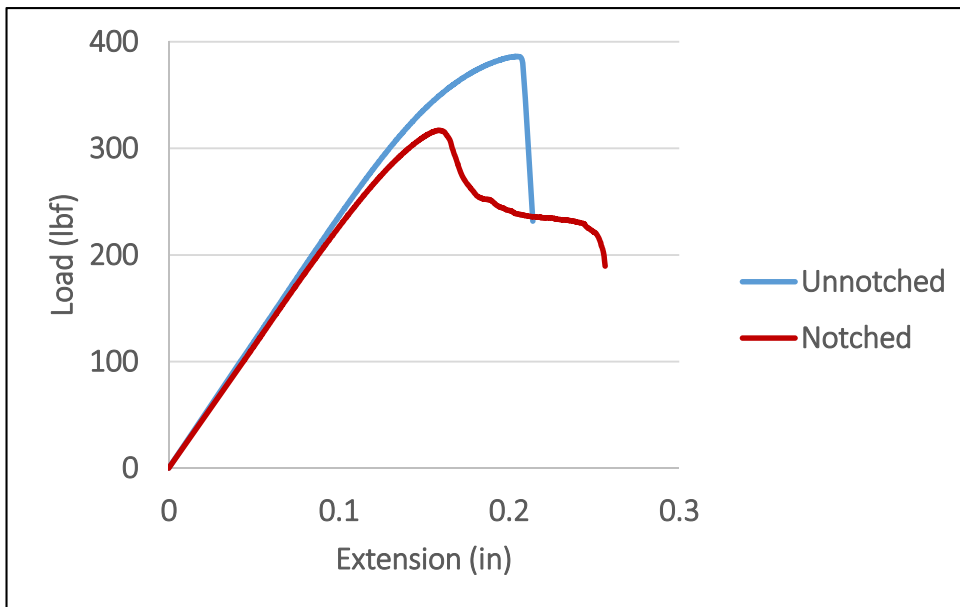


Notch

# Current Focus: Notched Core Shear Results

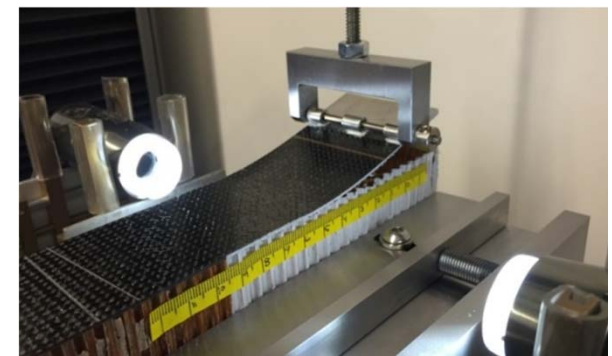
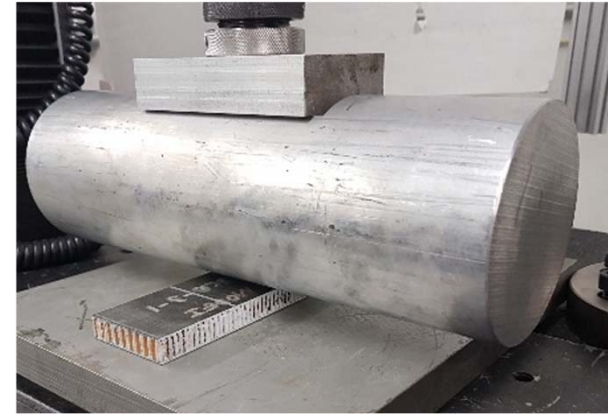
- Similar behavior between L and W core orientations
- Net section shear failure
- No significant notch effect observed

Direction	L	W
Notched Shear Strength Ratio	0.84	0.82
Notched Area Ratio (W-D)/W	0.83	



# Testing Considerations: Disbond After Indentation

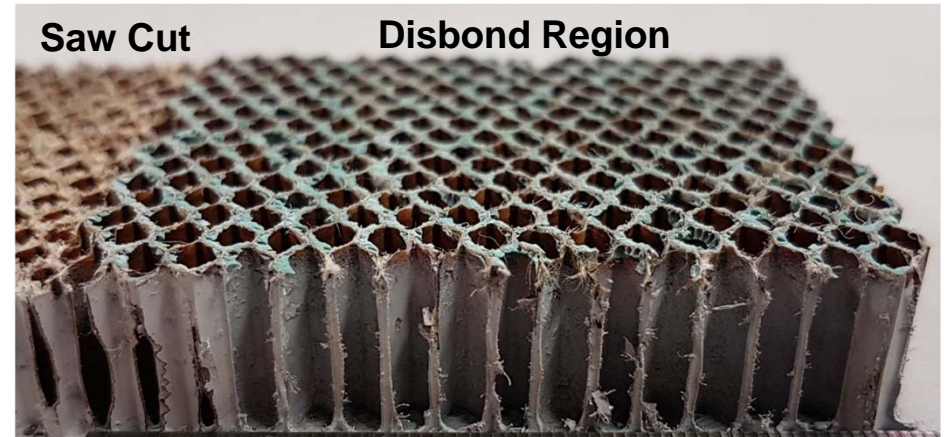
- **Quasi-static indentation**
  - Minimize facesheet damage
  - Produce region of crushed core
- **Indenter geometries**
  - Flat plate (uniform crush)
  - Wedge (tapered crush)
  - Cylinder (discreet crush region)
- **Mode I facesheet disbond testing following indentation**
  - Single Cantilever Beam (SCB) test
  - Fracture toughness reductions due to core crush
  - Thru-thickness failure locations and fracture surfaces



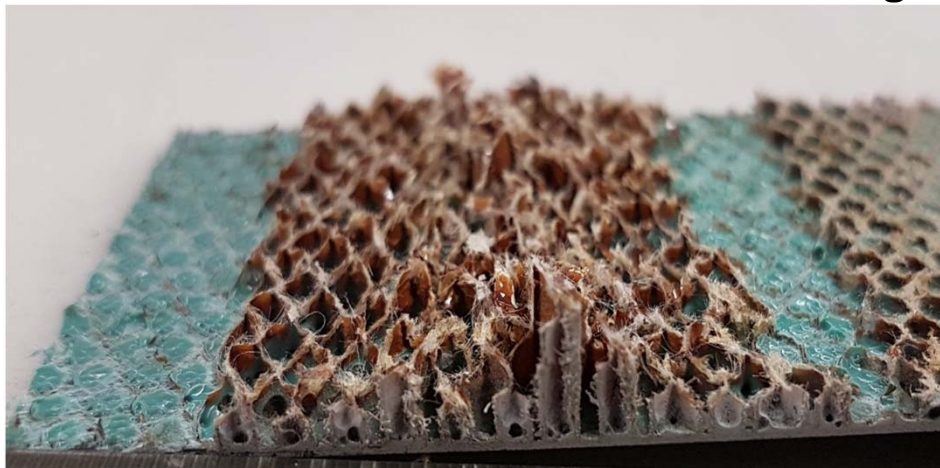
# Disbond After Indentation Testing: Fracture Path Through Core Crush Region

- Fracture at core/facesheet interface for undamaged core
- Fracture propagates along crushed core boundary in region of indentation

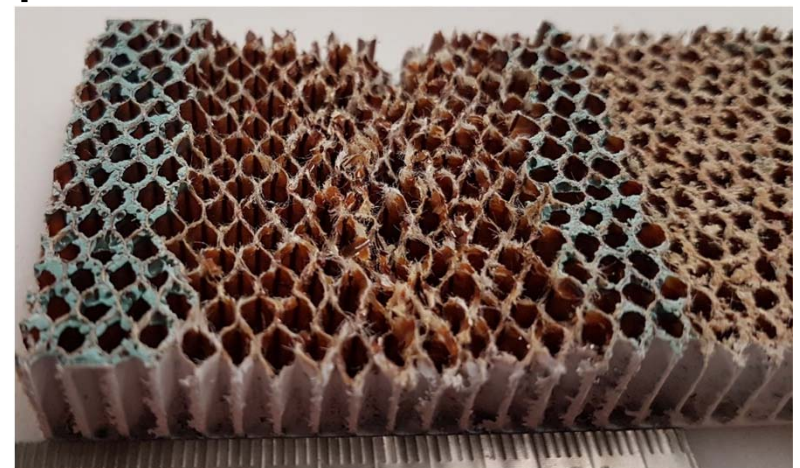
Undamaged 8 pcf Nomex core



Indentation Region, 8 pcf Nomex core



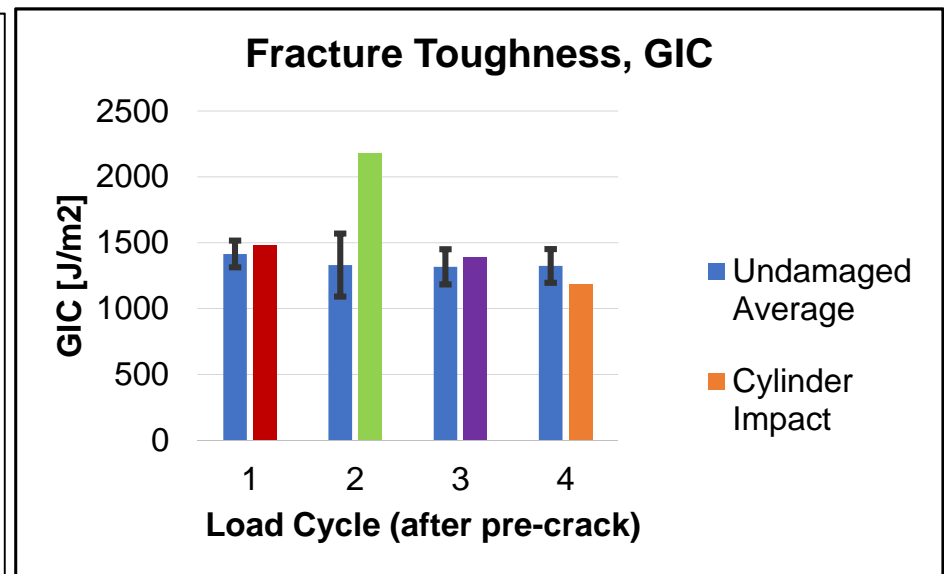
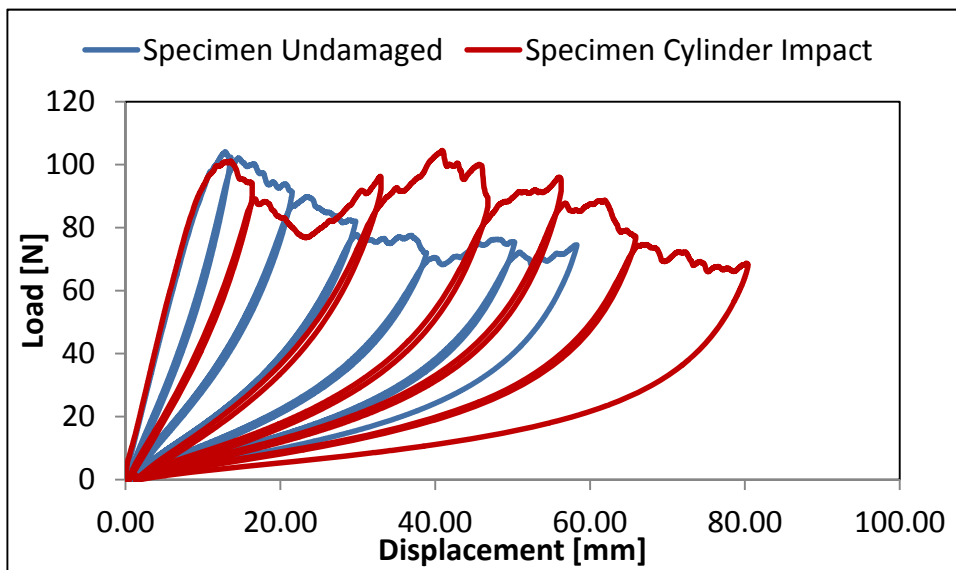
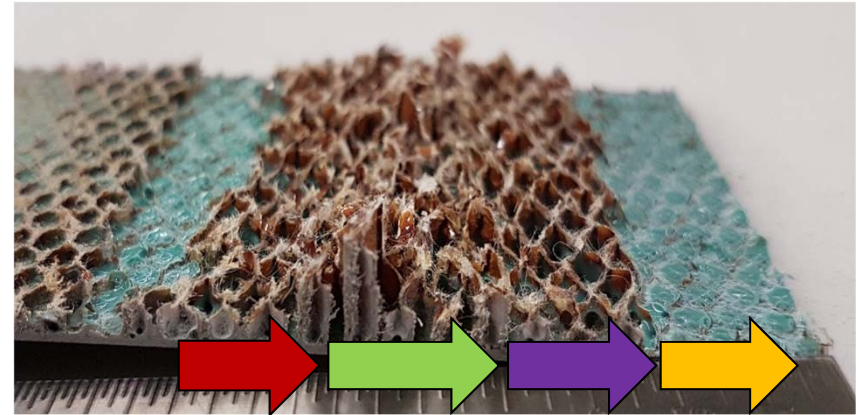
Top



Bottom

# Initial Test Results: Disbond After Indentation Testing

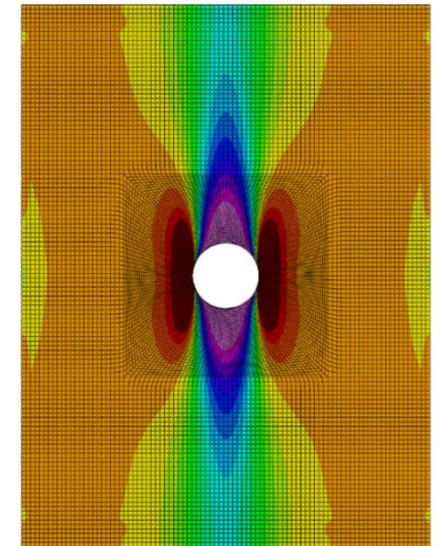
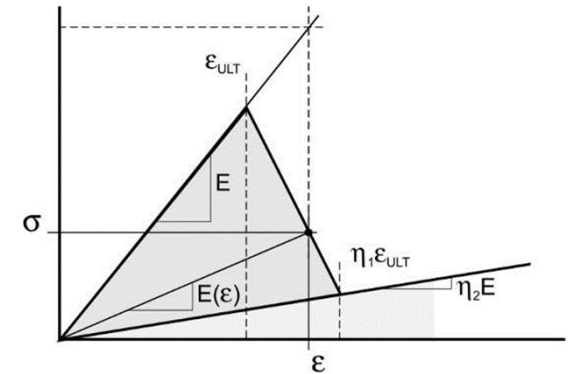
- Increased fracture toughness in regions of crushed core
- Highest  $G_{IC}$  obtained in central region of core crushing
- Further testing underway





# Analysis of Notched Sandwich Specimens ABAQUS with NDBILIN:

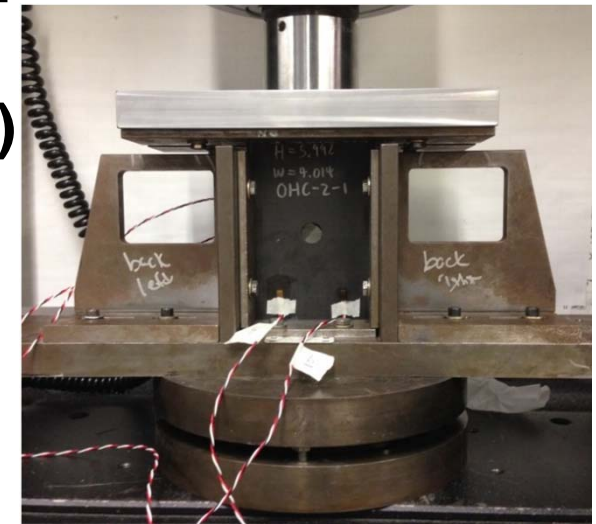
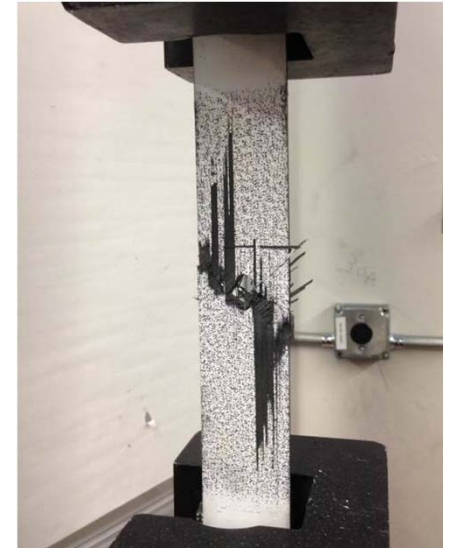
- User-defined nonlinear material model (UMAT) for ABAQUS
- Developed by Materials Sciences Corp.
- Stiffness degradation based progressive damage model
  - Bilinear stiffness response used to model material damaged state
  - “Built in” laminated plate theory for elements
  - Lamina level stiffness degradation
  - Max. stress, max. strain or Hashin failure criteria for damage onset



# Analysis of Notched Sandwich Specimens

## Validation of Modeling Approach

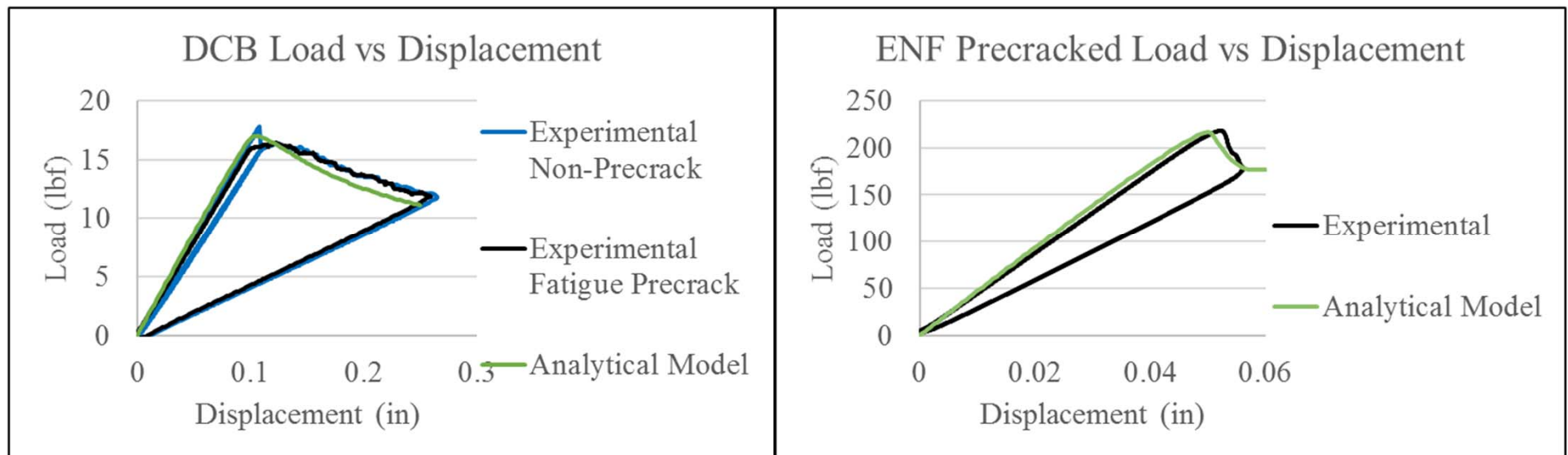
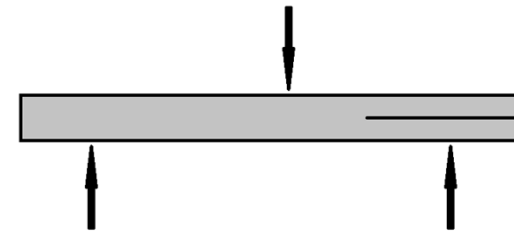
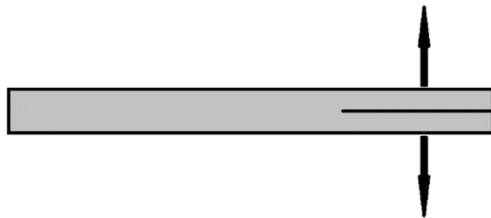
- **Modeling of damage progression in facesheets**
  - Interlaminar disbond (Mode I and II)
    - Cohesive Surfaces
  - Laminate tension (+/-45 layup)
  - Open-hole tension test
  - Open-hole compression test
- **Modeling of damage progression in sandwich composites**
  - Sandwich interface disbond (Mode I and II)
    - Cohesive Elements
  - Sandwich open-hole flexure
  - Sandwich open-hole shear
  - Sandwich open-hole compression



# Damage Progression in Facesheets: Interlaminar Disbond

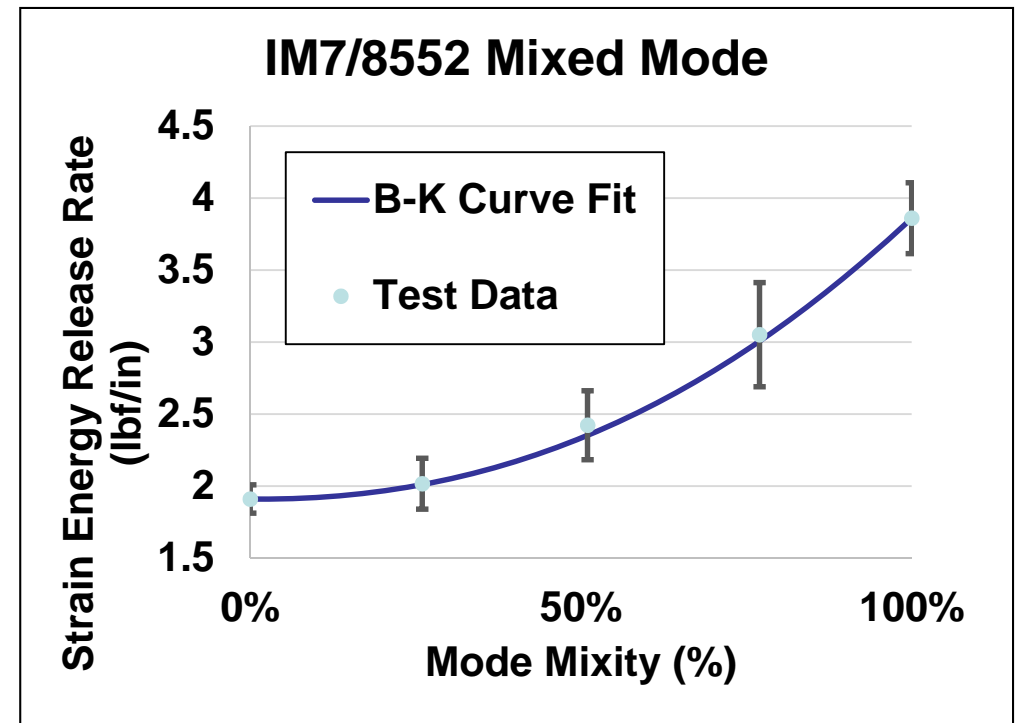
- **Calibration of interlaminar cohesive surfaces**

- Mode I DCB using ASTM D5528
- Mode II ENF using ASTM D7905



# Damage Progression in Facesheets: Mixed-Mode Interlaminar Disbond

- Calibration of interlaminar cohesive surfaces
  - Mixed-Mode Bend (MMB) using ASTM D6671
  - Fit using Benzeggagh-Kenane (B-K) criterion

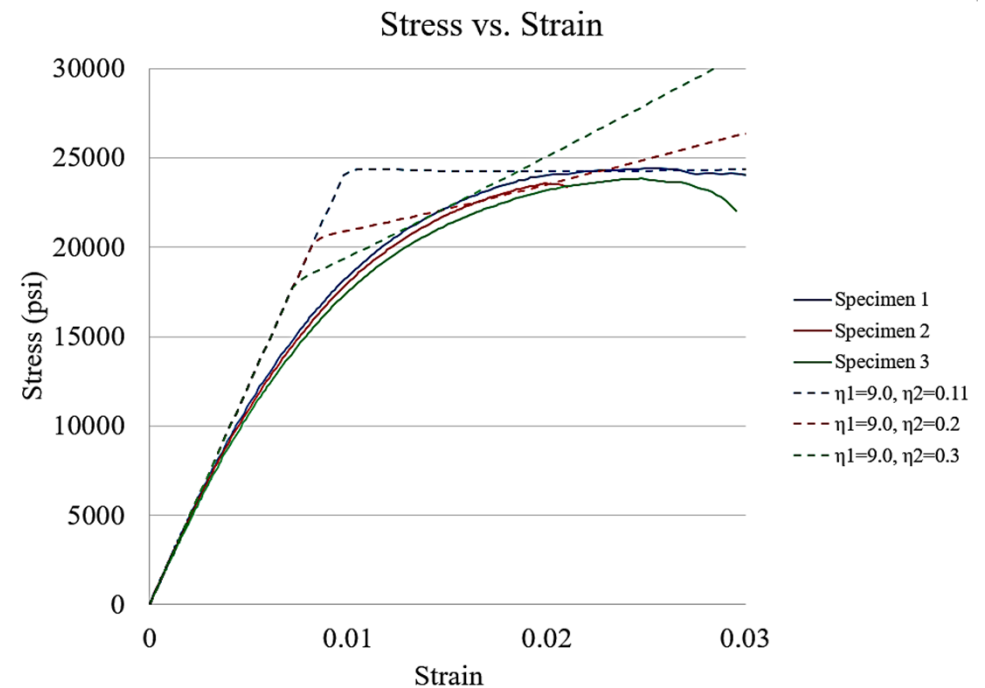
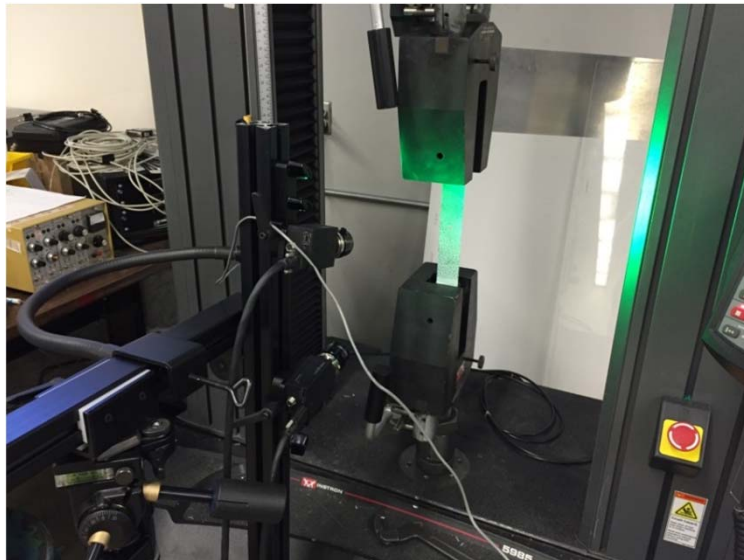


# Damage Progression in Facesheets: Analysis of +/-45 Laminates

- Simulation of tension testing of IM7/8552 carbon/epoxy laminates

$[45/-45]_{2s}$

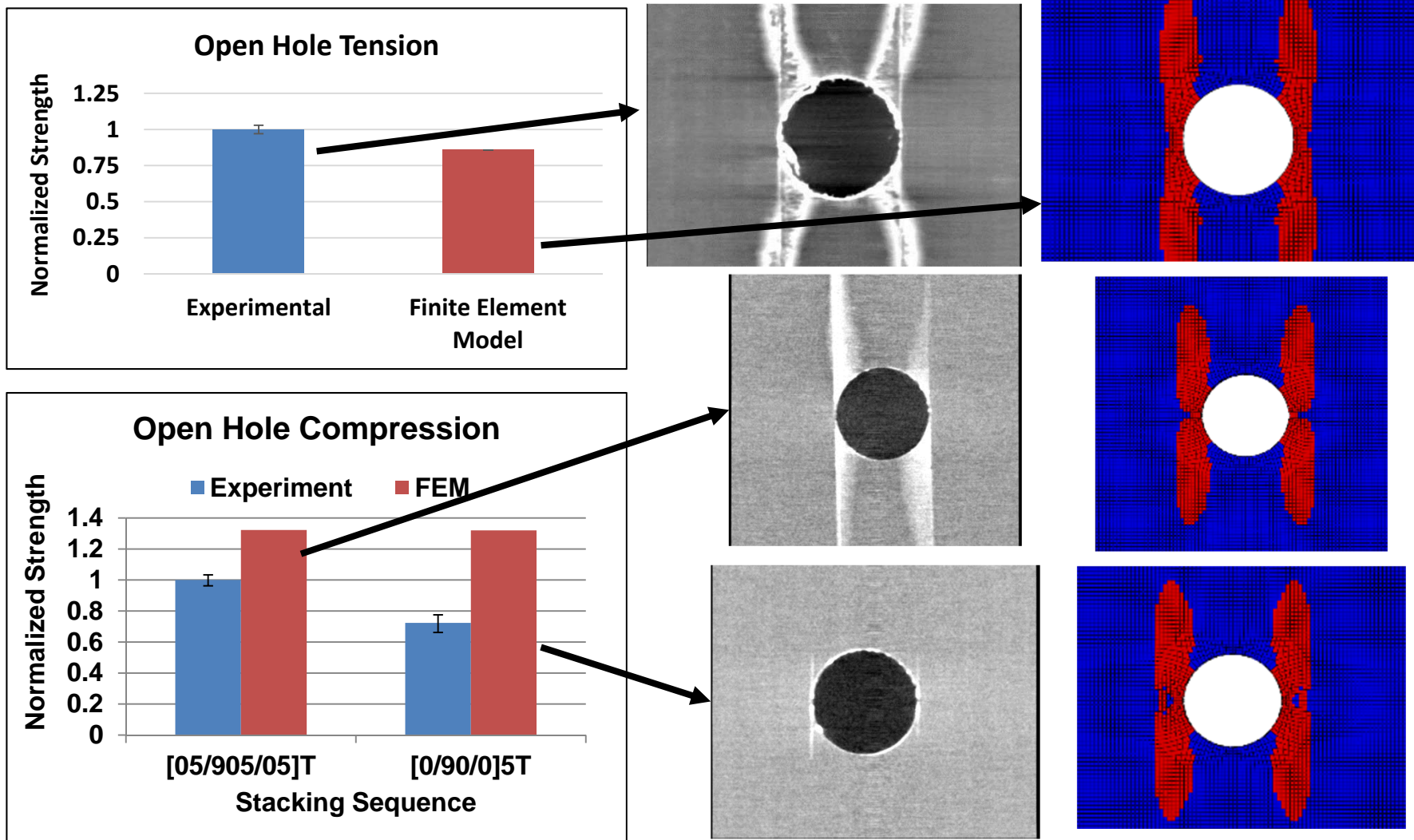
- NDBILIN matrix shear strength and damage parameters were modified to model test behavior



- Infinite potential solutions exist

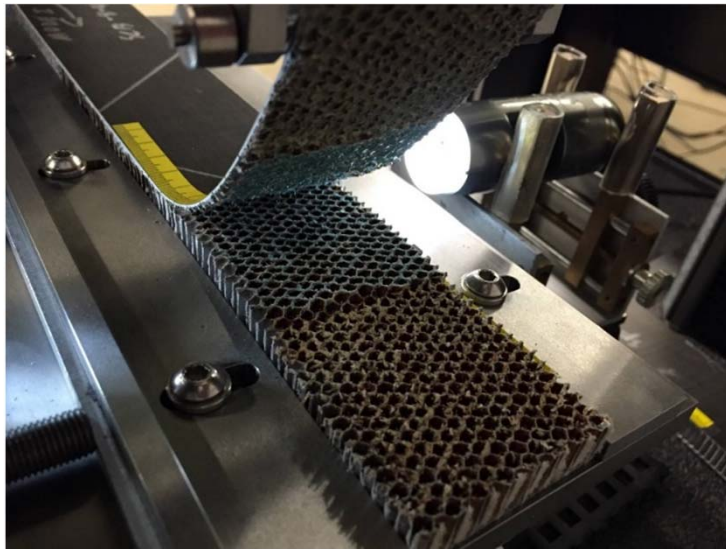
# Current Focus: Damage Progression in Facesheets

- Revisit open hole results with updated cohesive surface parameters and matrix damage parameters

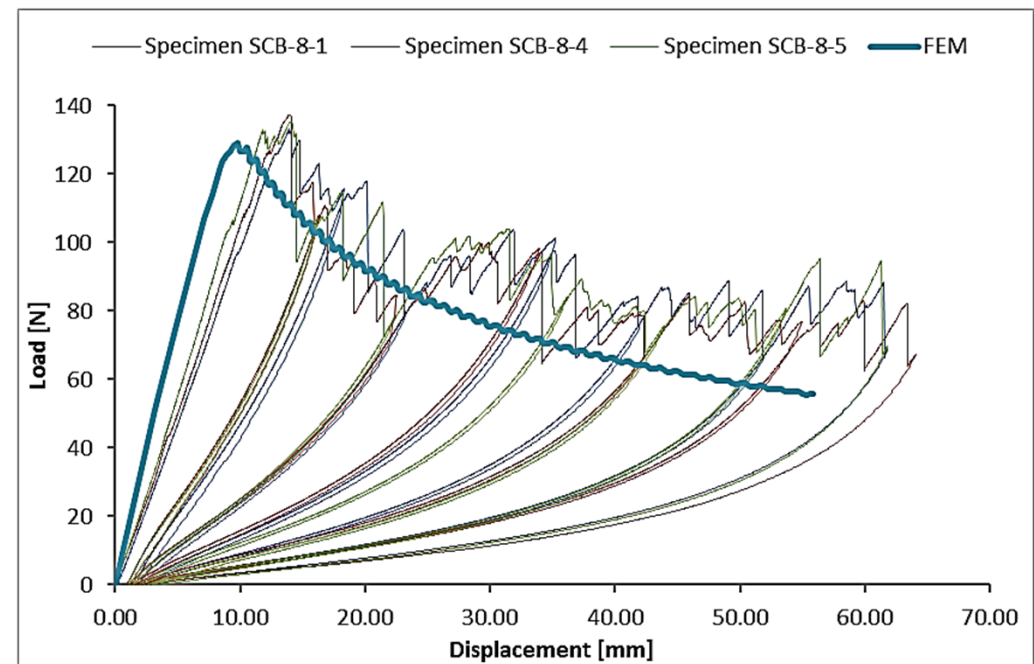


# Damage Progression in Sandwich Composites: Interface Disbond

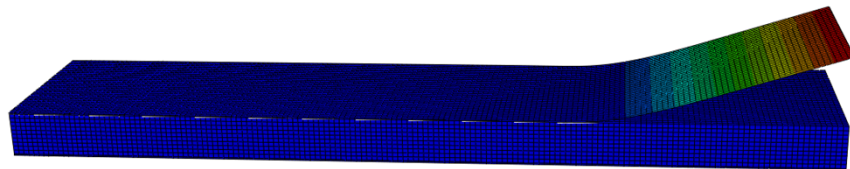
- Calibration of interfacial cohesive elements
  - Mode I Sandwich SCB



Single Cantilever Beam Test



Load vs Extension Data



Single Cantilever Model Displacements

# Damage Progression in Sandwich Composites: Mode II and Mixed-Mode

- **Calibration of interfacial cohesive elements**
  - Mode II and MMB
  - Cell buckling at crack tip, no crack growth
  - Analytical and numerical models do not account for constraint effect on honeycomb core



Mode II Sandwich ENF Test

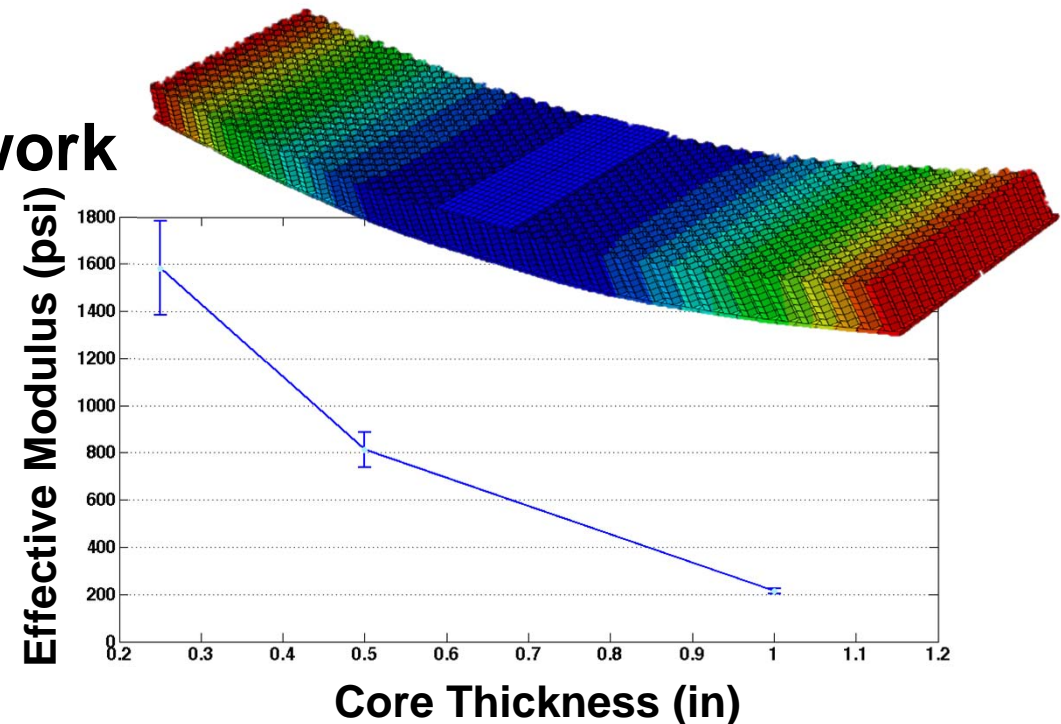
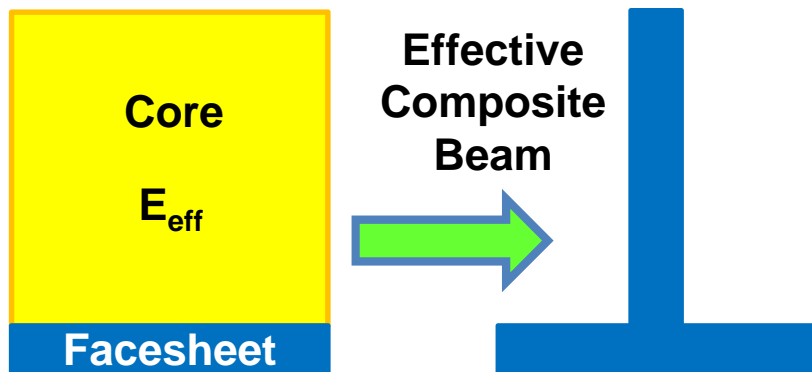
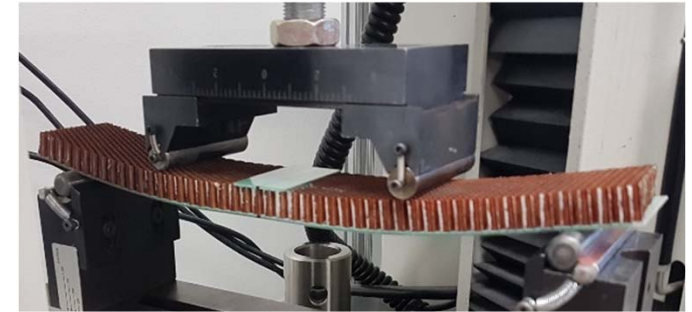


Sandwich Mixed Mode Bend Test



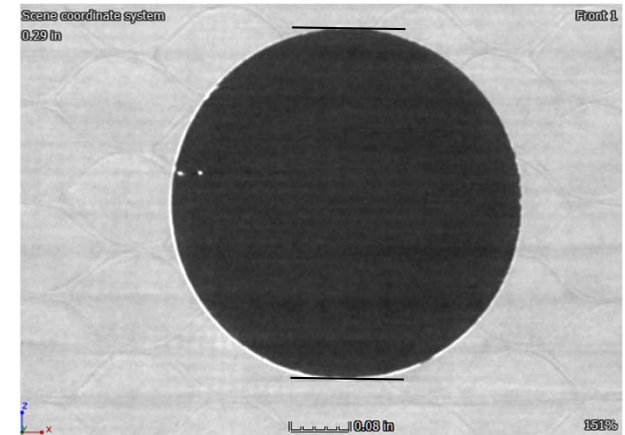
# Current Focus: Core Constraint Effect

- Open Face Flexure Tests
  - Nomex honeycomb core
  - Multiple core thicknesses
  - Core modeled explicitly
  - Homogeneous core in work



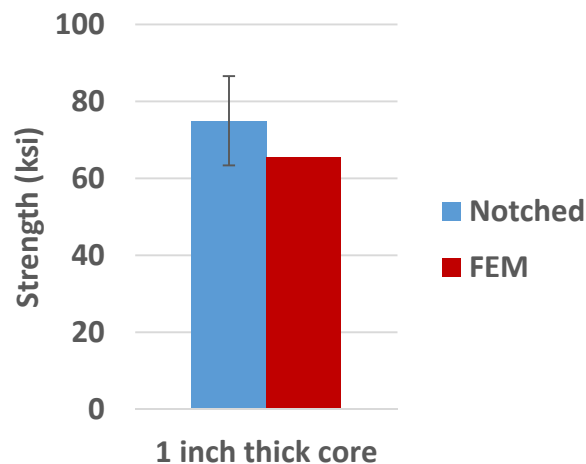
# Damage Progression in Sandwich Composites: Sandwich Open-Hole Flexure Test

- 90% load X-ray CT shows minimal damage progression
- Model over predicting damage progression and under predicting failure load

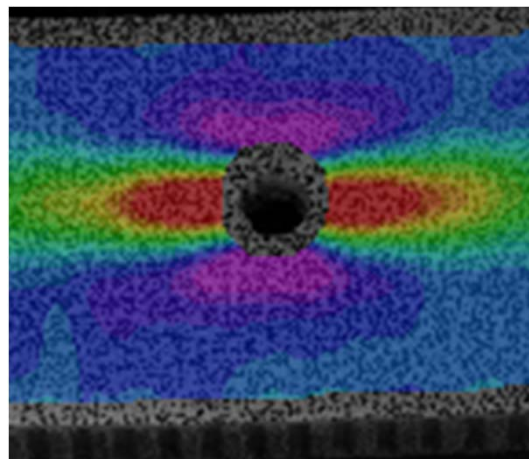


X-Ray CT

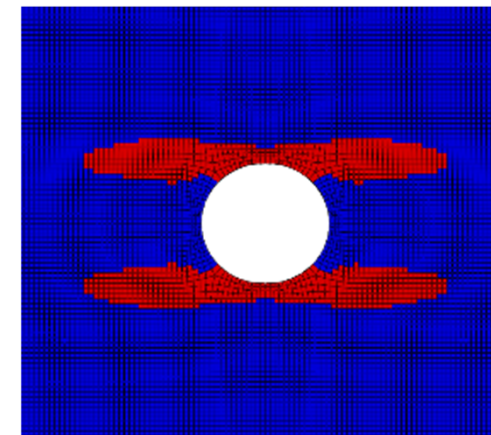
(Courtesy of Southwest Research Institute)



Compression Strength



DIC Strain



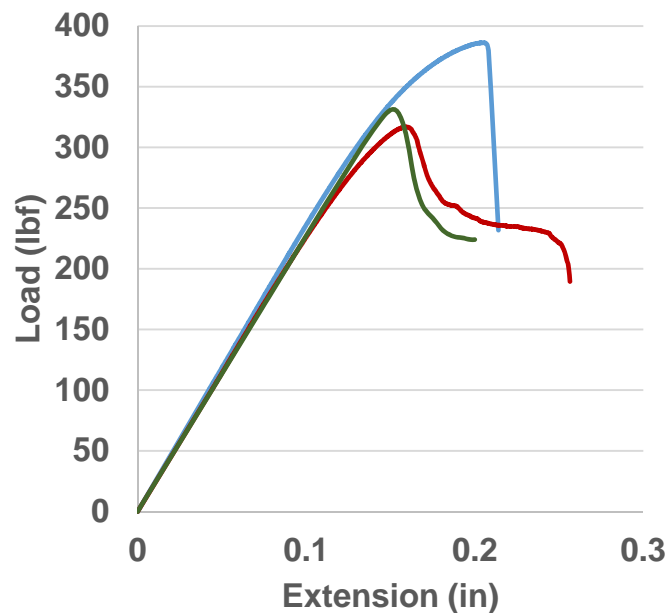
NDBILIN Damage Prediction

# Damage Progression in Sandwich Composites: Sandwich Open-Hole Shear Test

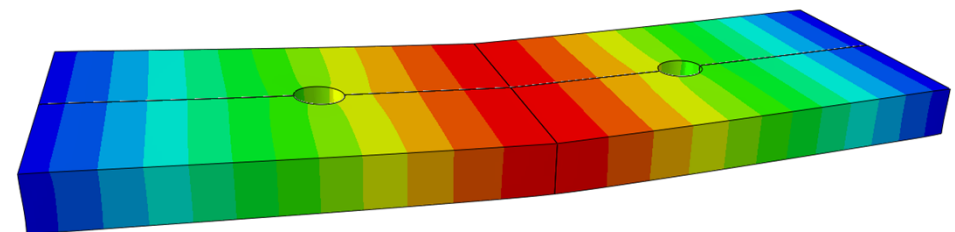
- Core modeled with NDBILIN
- Slight over prediction of max load
- Reload captured



Sandwich Open-Hole Shear Failure



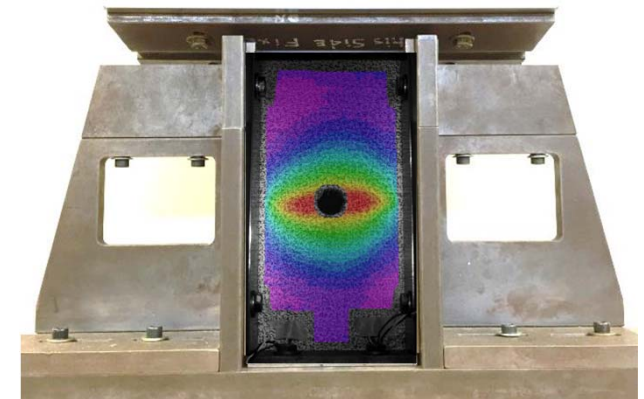
— Unnotched  
— Notched  
— NDBILIN



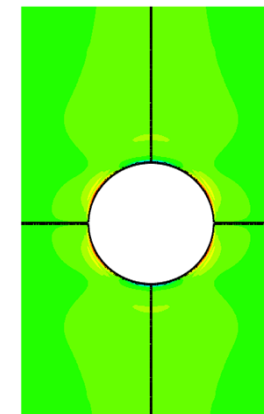
Model Displacements

# Damage Progression in Sandwich Composites: Sandwich Open-Hole Compression Test

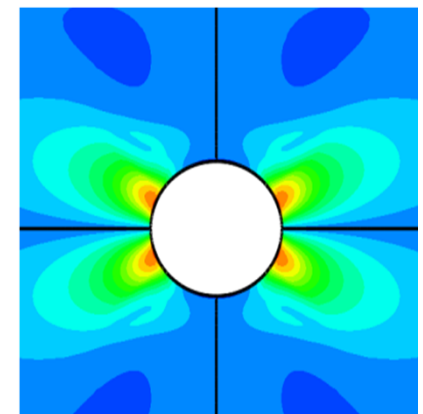
- Out-of-plane displacement observed in DIC measurements
- First mode facesheet buckling observed
- Investigating facesheet buckling using ABAQUS Riks
- Zero thickness cohesive elements caused numerical errors during perturbation step
- Cohesive surfaces implemented
- Non-linear vs Riks shows a large increase in cohesive stress



Out-of-plane deformation



Non-Linear



Riks

# Future Work:

## Notch Sensitivity of Composite Sandwich Structures

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- **Development of sizing guidelines for sandwich open hole compression and flexure tests**
- **Incorporate updated material/model parameters in laminate open hole tension/compression simulations**
- **Explore implementation of homogeneous core for Mode II and MMB**
- **Incorporate initial disbond with Teflon inserts to validate buckling model**

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# Thank you for your attention!

## Questions?

