

The logo for the Joint Advanced Materials and Structures Center of Excellence (JAMS) features the letters 'JAMS' in a bold, blue, textured font. The letters are set against a background of two curved, overlapping bands: a yellow band on top and a dark blue band on the bottom, both tapering towards the right side of the slide.

JAMS

Damage Tolerance Testing and Analysis Protocols for Full-Scale Composite Airframe Structures Under Repeated Loading

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Executive Director, NIAR and
Sam Bloomfield Distinguished Professor of Aerospace Engineering

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Sr. Research Engineer, NIAR

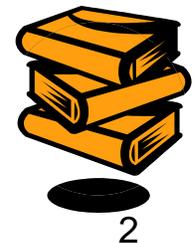


The Joint Advanced Materials and Structures Center of Excellence

- Produce a guideline FAA document, which demonstrates a “best practice” procedure for full-scale testing protocols for composite airframe structures with examples



- Although the materials, processes, layup, loading modes, failure modes, etc. are significantly different, most of current certification programs use the **load-life factors generated for NAVY F/A-18 program**.
 - Guidance to ensure safe reliable approach
 - Correlate certified “life” to improved LEF (load-life shift)
- With increased use of composite materials in primary structures, there is **growing need to investigate extremely improbable high energy impact threats** that reduce the residual strength of a composite structure to limit load.
 - Synthesize damage philosophy into the scatter analysis
 - Multiple LEF for different stage of test substantiation

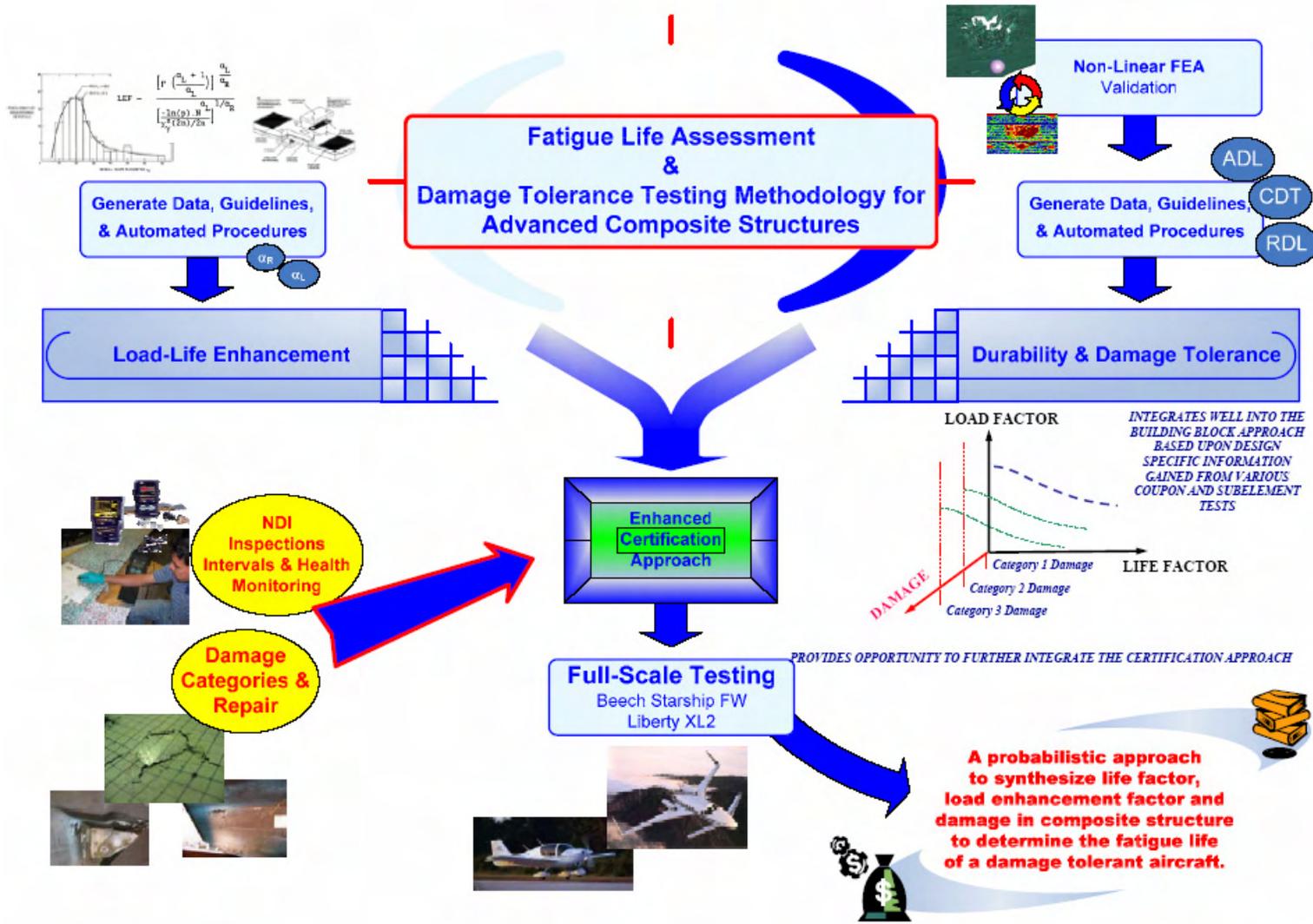


Primary Objective

- Develop a probabilistic approach to synthesize life factor, load factor and damage in composite structure to **determine fatigue life of a damage tolerant aircraft**
 - *Demonstrate acceptable means of compliance for fatigue, damage tolerance and static strength substantiation of composite airframe structures*
 - Evaluate existing analysis methods and building-block database needs as applied to practical problems crucial to composite airframe structural substantiation
 - Investigate realistic service damage scenarios and the inspection & repair procedures suitable for field practice

Secondary Objectives

- Extend the current certification approach to **explore extremely improbable high energy impact threats**, i.e. damages that reduce residual strength of aircraft to limit load capability
 - Investigate realistic service damage scenarios
 - Inspection & repair procedures suitable for field practice
- Incorporating certain **design changes** into full-scale substantiation without the burden of additional time-consuming and costly tests



JAMS FAA Sponsored Project Information



- **Principal Investigators**
 - Dr. John Tomblin and Waruna Seneviratne
- **FAA Technical Monitor**
 - Curt Davis
- **Other FAA Personnel Involved**
 - Dr. Larry Ilcewicz
 - Peter Shyprykevich (consultant ret. FAA)



- **Industry Participation**



**Workshops for Composite
Damage Tolerance & Maintenance**

- 2008 CMH-17: PMC Forum & DTTG Meeting
- 2007 FAA/CACRC/EASA - Amsterdam, Netherlands
- 2006 FAA Workshop - Chicago, IL



*We all think about
 these
 applications ...
 but ...*

Other Applications of Advanced Materials



Cirrus



Lancair



Spectrum



Horizon



Adam Aircraft



Javelin



Premier I



Predator



Epic



Honda



Bell Helicopter



Global Hawk



SpaceshipOne

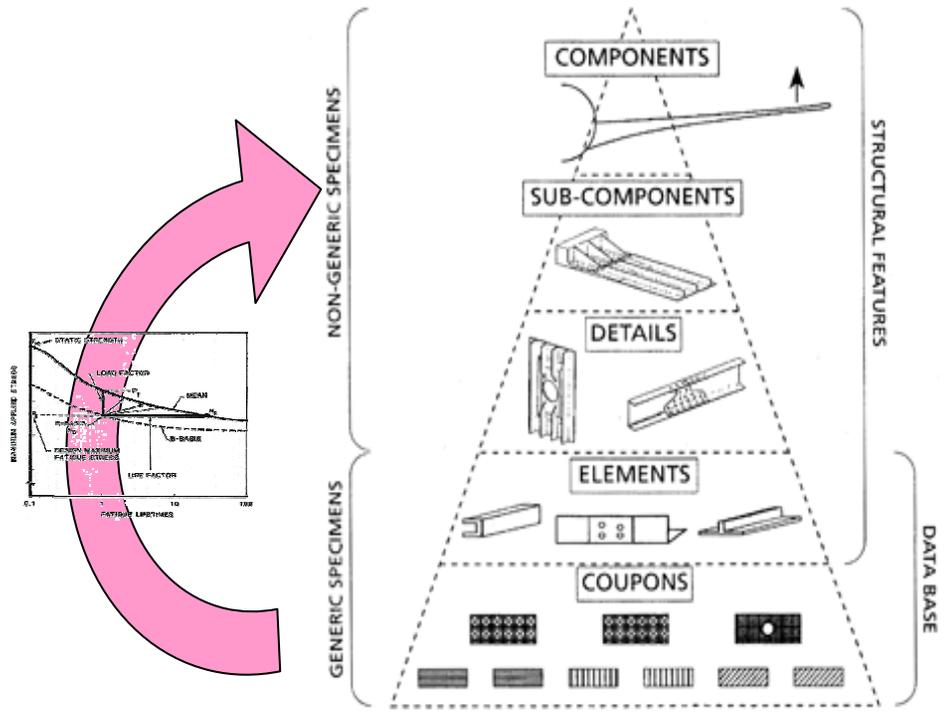


Liberty



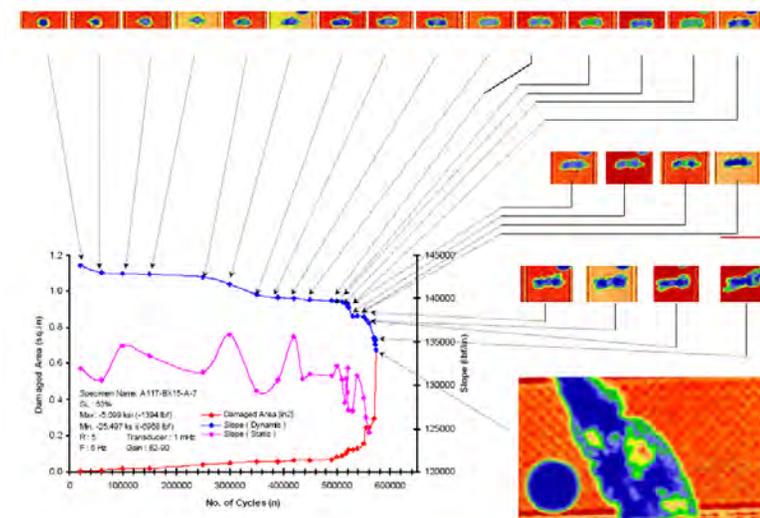
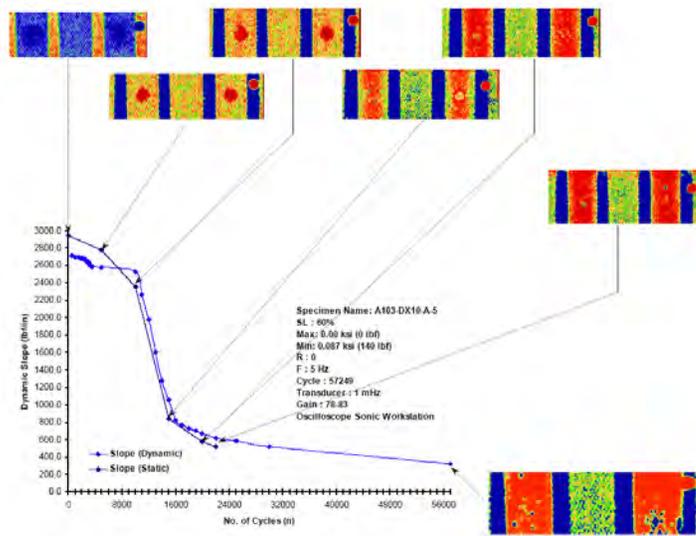
Toyota Aircraft

- Background – most test programs reference the Navy/FAA reports by Whitehead, *et. al.*, (1986) and follow that approach
 - Most test programs have used the conclusions developed in this report regardless of design features, failure modes and/or materials
- EADS-CASA study used the same approach (2001) but redefined the shape factors



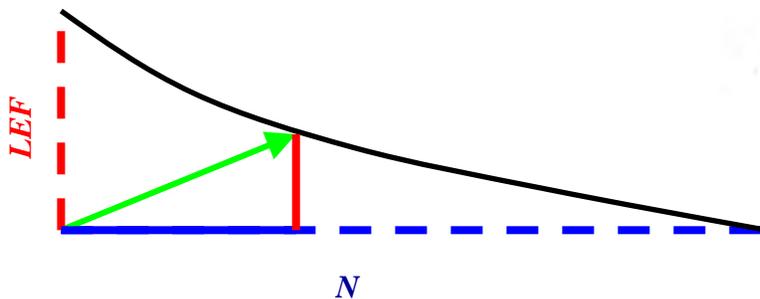
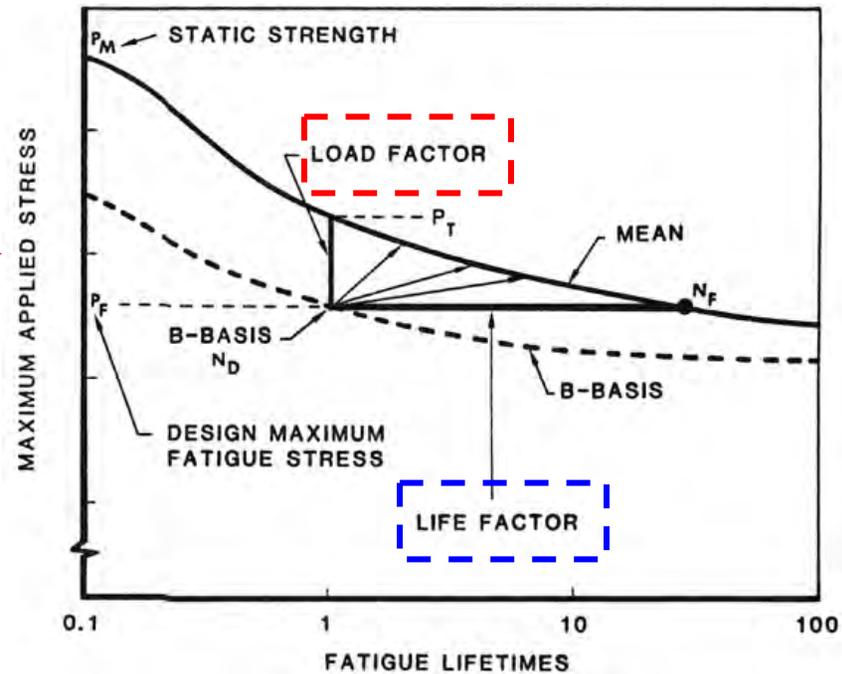
Integrates well into building-block approach based upon design-specific information gained from various coupon and element

- Complex failure modes
- Require extensive NDI
- Variable B-basis (scatter) at different stress levels
- Compliance change is a function of material, layup, test environment, loading mode, stress level, etc.



JAMS Load-Life Combined Approach

Increase applied loads in fatigue tests so that the **same level of reliability** can be achieved with a shorter test duration



Structure is tested for additional fatigue life to achieve the **desired level of reliability**

– FAA-LEF

- » AS4/E7K8 PW
- » T700/#2510 PW
- » 7781/#2510 8HS

– FAA-Laminate

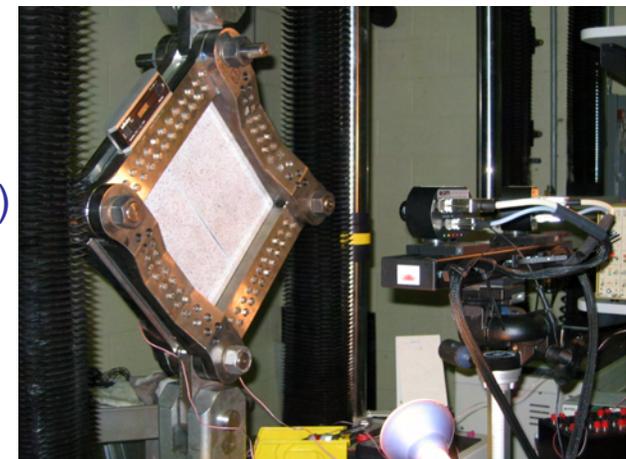
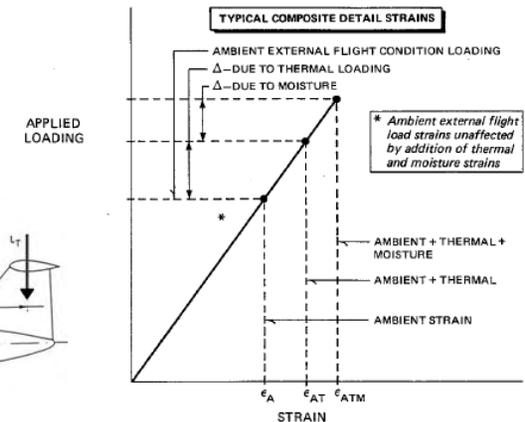
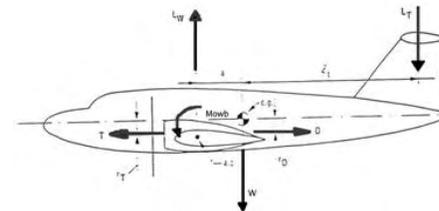
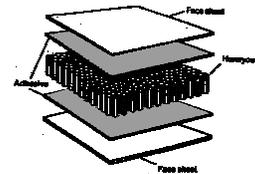
- » T700/#2510 UNI
- » T700/#2510 PW
- » T700/E765 UNI
- » T300/E765 PW
- » AS4C/MTM45 UNI
- » AS4C/MTM45 8HS

– FAA-Adhesive Fatigue

- » Loctite Paste
- » PTM&W paste (two bondline thicknesses)
- » EA 9696 film

– FAA-Adhesive Effects of Defects

- » T700/#2510 PW & EA9394

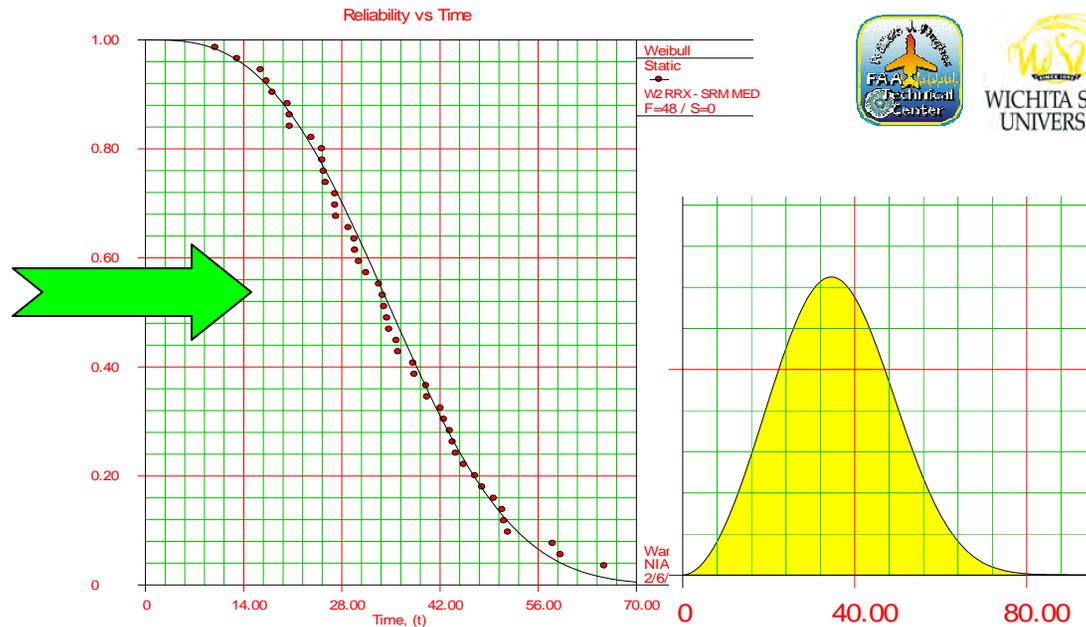




Laminate Statistical Allowable Generation for Fiber-Reinforced Composite Materials: Lamina Variability Method

[DOT/FAA/AR-06/53]

40/20/40	Single Shear Bearing-Tension -- (RTD)	45.4085
	Double Shear Bearing-Tension -- (RTD)	49.696
	Bearing-Bypass 50%-Tension	43.4258
	Bearing-Bypass 50%-Compression	42.102
	Bearing-Bypass 50%-Tension [t/D=0.475]	40.0401
	Bearing-Bypass 50%-Tension [t/D=0.570]	42.5935
	Bearing-Bypass 50%-Tension [t/D=0.949]	38.1976
	Open Hole-Tension [w/D=6]	27.2021
	Filled Hole-Tension	20.2959
	No Hole-Tension	29.8203
	No Hole-Compression	20.5843
	Open Hole-Compression	30.4534
	Critical Hole-Tension -- (CTD)	29.9075
	Critical Hole-Tension -- (ETD)	25.1923
	V-Notched Rail Shear	59.2079
	Open Hole-Tension [w/D=3]	20.594
	Open Hole-Tension [w/D=4]	27.0538
	Open Hole-Tension [w/D=8]	25.4413
25/50/25	Double Shear Bearing-Tension -- (CTD)	25.7206
	Double Shear Bearing-Tension -- (RTD)	43.8267
	Double Shear Bearing-Tension -- (ETW)	34.7752
	Single Shear Bearing-Tension -- (CTD)	28.956
	Single Shear Bearing-Tension -- (RTD)	18.1315
	Single Shear Bearing-Tension -- (ETW)	33.8501
	Bearing-Bypass 50%-Tension	44.2636
	Bearing-Bypass 50%-Compression	48.0284
	Open Hole-Tension [w/D=6] -- (CTD)	35.8156
	Open Hole-Tension [w/D=6] -- (RTD)	34.0488
	Open Hole-Tension [w/D=6] -- (ETW)	25.2227
	No Hole-Tension -- (CTD)	51.1531
	No Hole-Tension -- (RTD)	40.1864
	No Hole-Tension -- (ETW)	38.383
	No Hole-Compression -- (CTD)	31.498
	No Hole-Compression -- (RTD)	27.0743
	No Hole-Compression -- (ETW)	23.6762
	Open Hole-Compression -- (CTD)	34.4747
	Open Hole-Compression -- (RTD)	46.9989
	Open Hole-Compression -- (ETW)	33.3186
	V-Notched Rail Shear	16.4582
10/80/10	Bearing-Bypass 50%-Tension	65.4454
	Bearing-Bypass 50%-Compression	74.3601
	Open Hole-Tension [w/D=6]	51.7133
	No Hole-Tension	58.0843
	No Hole-Compression	36.0558
	Open Hole-Compression	50.909
	V-Notched Rail Shear -- (CTD)	9.9634
	V-Notched Rail Shear -- (RTD)	17.2784
	V-Notched Rail Shear -- (ETW)	13.1027



T700SC-12K-50C/#2510 -Plain Weave Fabric

863 specimens

α 2.941
 β 39.836

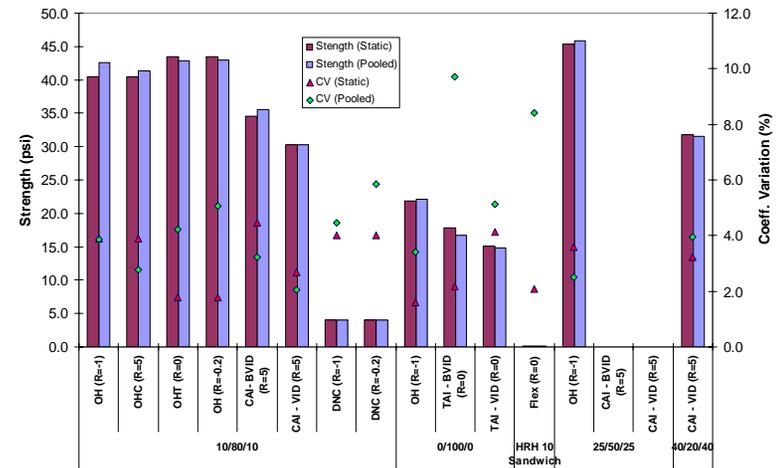
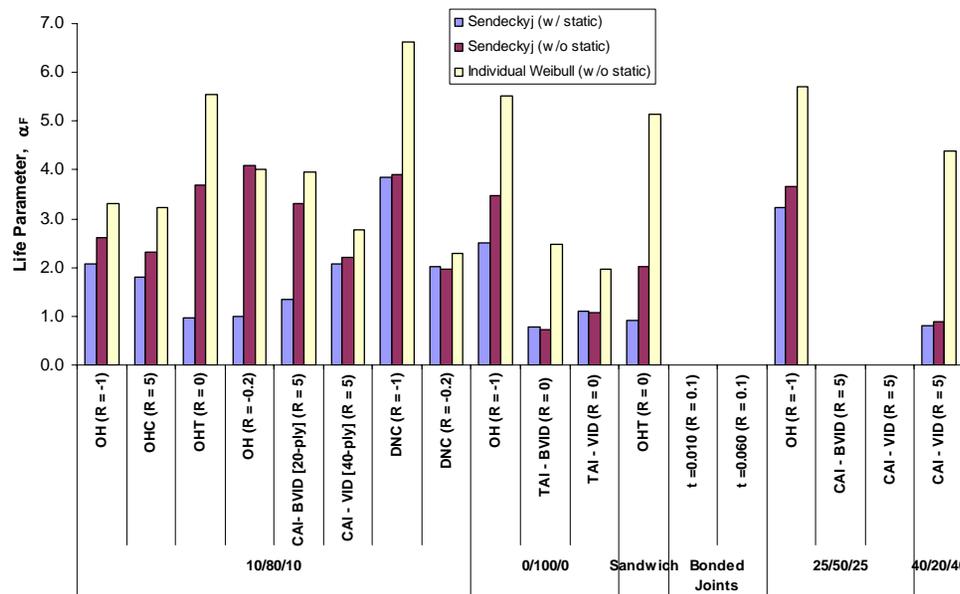
MODAL (EXTREAM)

α_R 34.587

Fatigue Scatter Analysis Techniques

- Individual Weibull
- Joint Weibull
- Sedecyjk Equivalent Strength Model

Data Pooling Techniques



NADC Fatigue Scatter Analysis

$$\alpha_i > \alpha_j > \alpha_s$$

Shape Parameters for Fatigue Data [2, 5, and 10 -Hz combined]

w/ Static Data

	CTD	RTD	RTW	# of Specs.
Loctite	0.805	0.662	0.682	95
EA9696	0.847	0.403	0.379	103
PTM&W (0.06")	0.870	1.051	0.681	101
PTM&W (0.16")	0.363	0.856	0.671	91

Total 390

α 3.8538

β 0.7641

Modal Value 0.707

w/o Static Data (Sendecky)

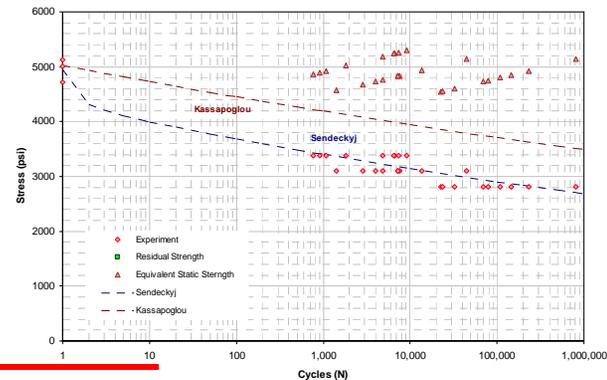
	CTD	RTD	RTW	# of Specs.
Loctite	0.821	1.624	0.644	86
EA9696	4.119	1.389	2.189	88
PTM&W (0.06")	1.376	1.483	1.169	92
PTM&W (0.16")	0.669	4.296	1.618	82

Total 348

α 1.6789

β 2.016

Modal Value 1.176



w/o Static Data (Individual Weibull)

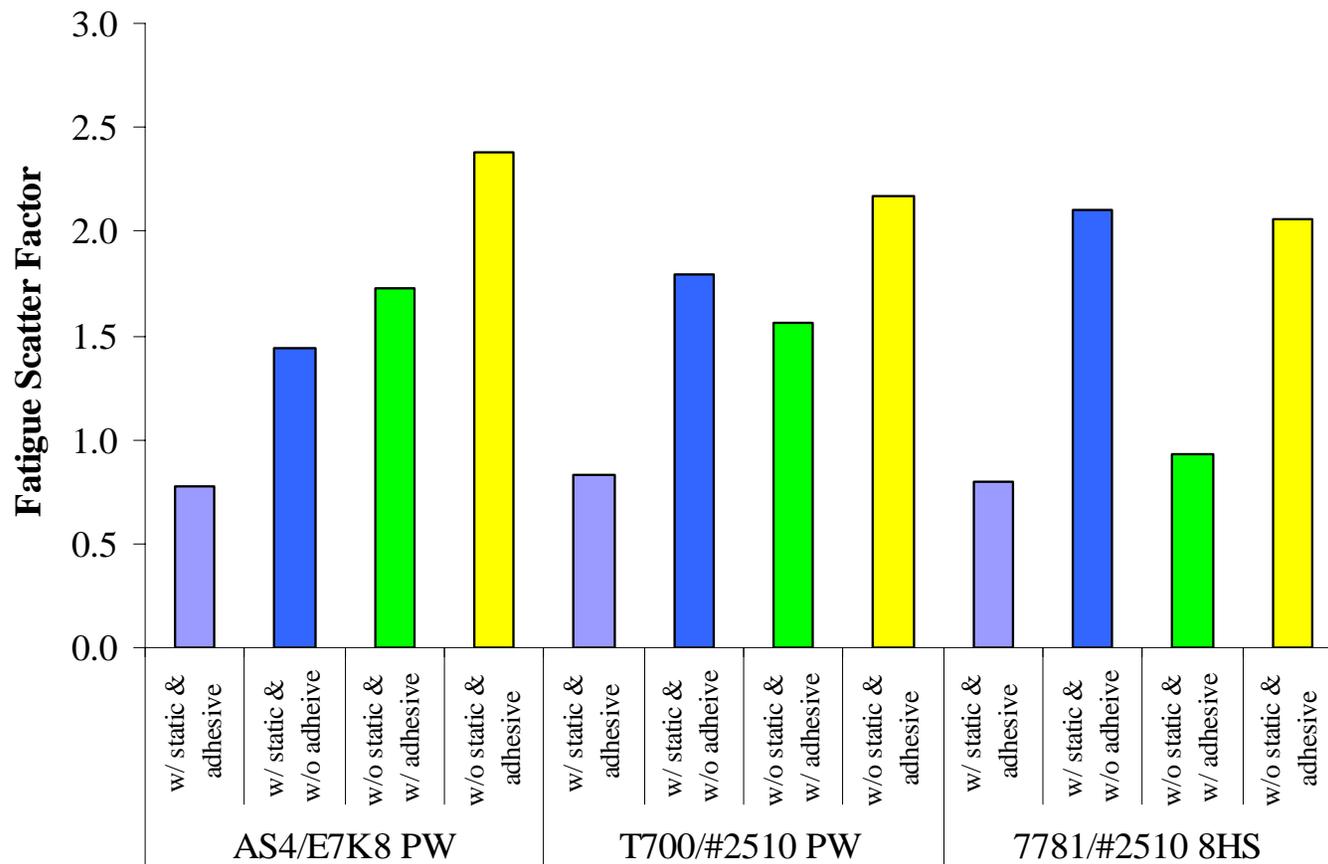
	CTD	RTD	RTW
Loctite	1.069	1.226	1.109
EA9696	2.372	2.077	1.110
PTM&W (0.06")	1.541	1.179	1.417
PTM&W (0.16")	1.165	2.170	1.061

α 3.3394

β 1.6255

Modal Value 1.461

Life Scatter Summary





FAA-LEF Calculations

File Edit About

INPUT VALUES

Zigma A	n	Zigma R
110	49800	169
110	138180	254
110		287
85	93880	
85	224630	
85		
85	55780	
70	464810	
70		
70	112231	
70	0	
55	211800	
55		

GET INPUT >>

OUTPUT
 Selected All

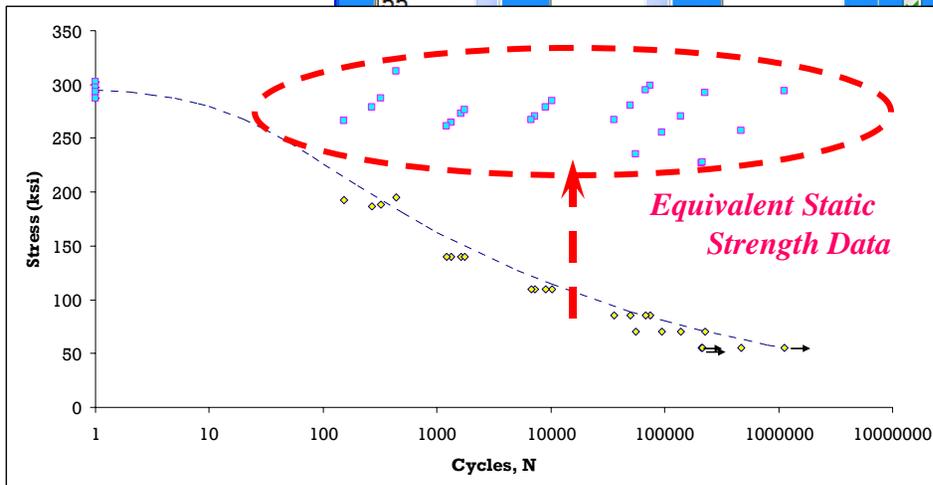
CONDITION
 Z1 > Z2 > Z3
 (Z1 + Z3)/2 < Z2
 NONE

OUTPUT PARAMETERS
 Zigma 1 Index I
 Zigma 2 Index J
 Zigma 3 Index K
 Alpha Hat C0
 Beta Hat S0

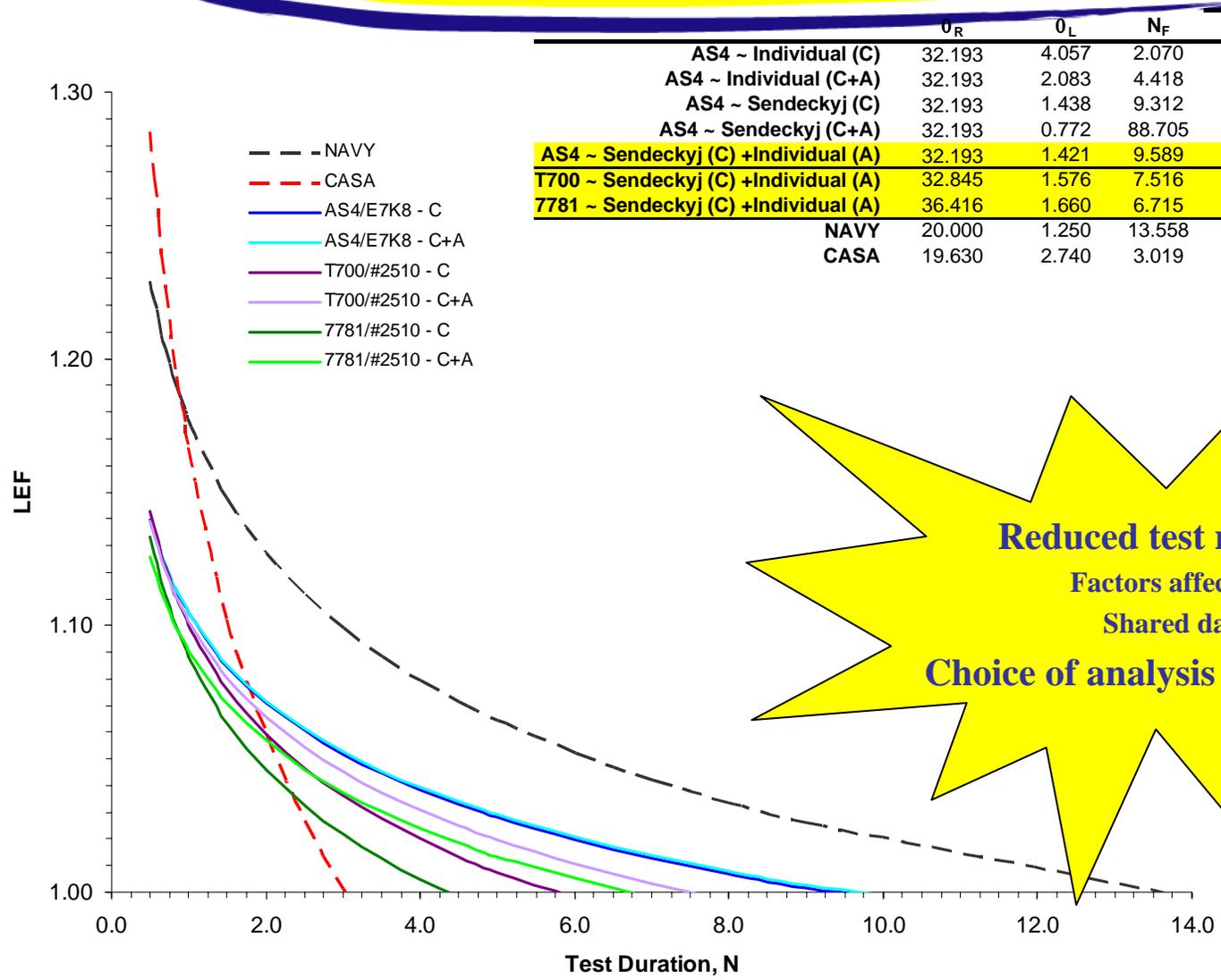
GENERATE

PROCESSING VALUES

Zigma A	n	Zigma R
302	1	169
297	1	254
293	1	287
287	1	
193	153	
187	267	
188	319	
195	436	
140	1630	
140	1330	
140	1760	
140	1220	
110	10200	
110	9000	
110	7290	
110	6750	
85	74250	
85	67490	
85	36210	
85	49800	
70	138180	
70	93880	

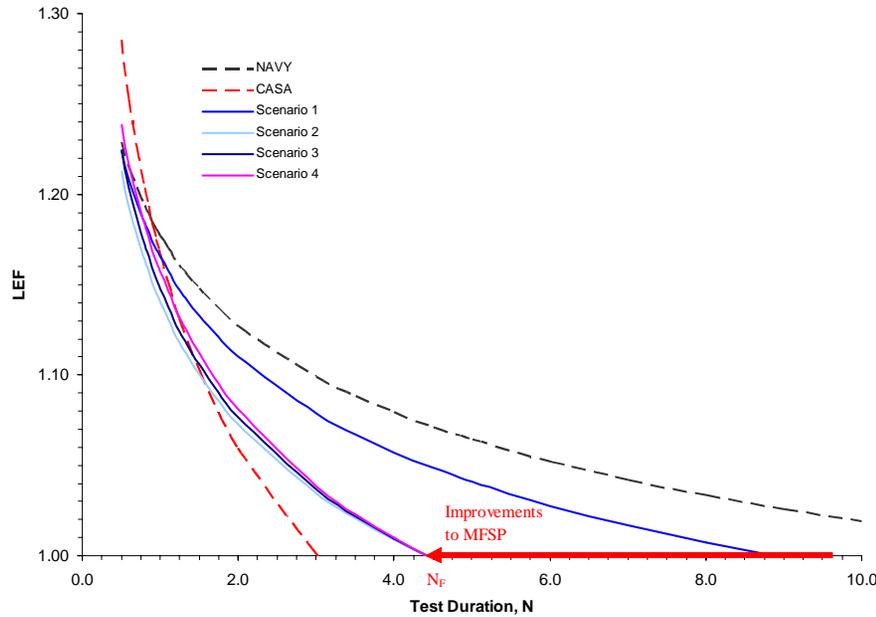


$$LEF = \frac{\left[\Gamma \left(\frac{\alpha_L + 1}{\alpha_L} \right) \right]^{\frac{\alpha_L}{\alpha_R}}}{\left[\frac{-\ln(p) \cdot N}{\chi^2(2n)/2n} \right]^{\frac{1}{\alpha_R}}}$$



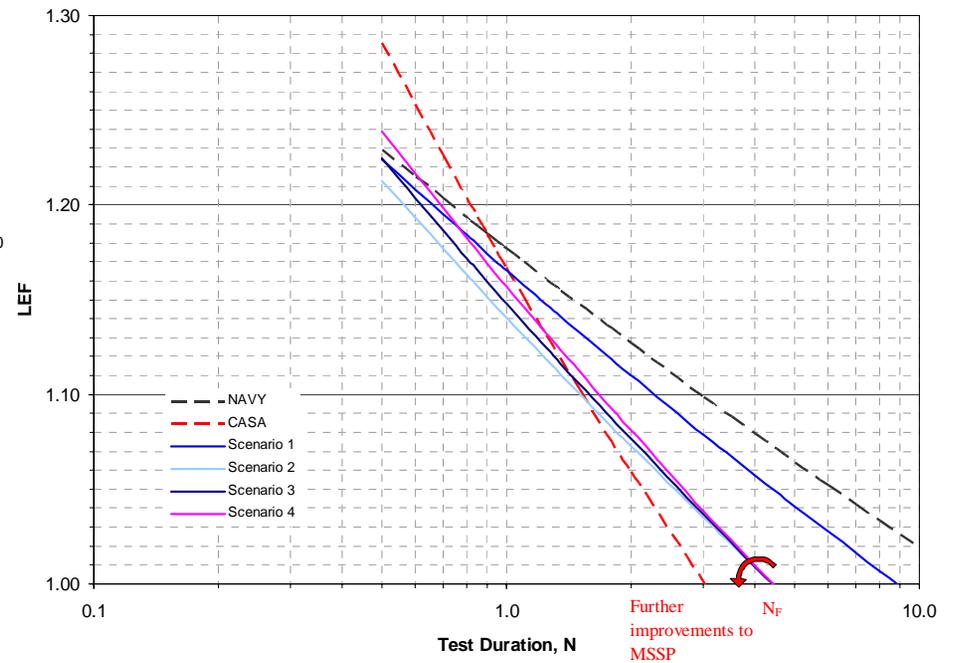
	0_R	0_L	N_F	0.5	1.0	1.5	3.0
AS4 ~ Individual (C)	32.193	4.057	2.070	1.196	1.096	1.041	0.954
AS4 ~ Individual (C+A)	32.193	2.083	4.418	1.151	1.101	1.072	1.025
AS4 ~ Sendeckyj (C)	32.193	1.438	9.312	1.140	1.105	1.085	1.052
AS4 ~ Sendeckyj (C+A)	32.193	0.772	88.705	1.132	1.114	1.103	1.085
AS4 ~ Sendeckyj (C) + Individual (A)	32.193	1.421	9.589	1.139	1.105	1.085	1.053
T700 ~ Sendeckyj (C) + Individual (A)	32.845	1.576	7.516	1.139	1.102	1.080	1.045
7781 ~ Sendeckyj (C) + Individual (A)	36.416	1.660	6.715	1.126	1.091	1.071	1.037
NAVY	20.000	1.250	13.558	1.229	1.177	1.148	1.099
CASA	19.630	2.740	3.019	1.285	1.167	1.103	1.001

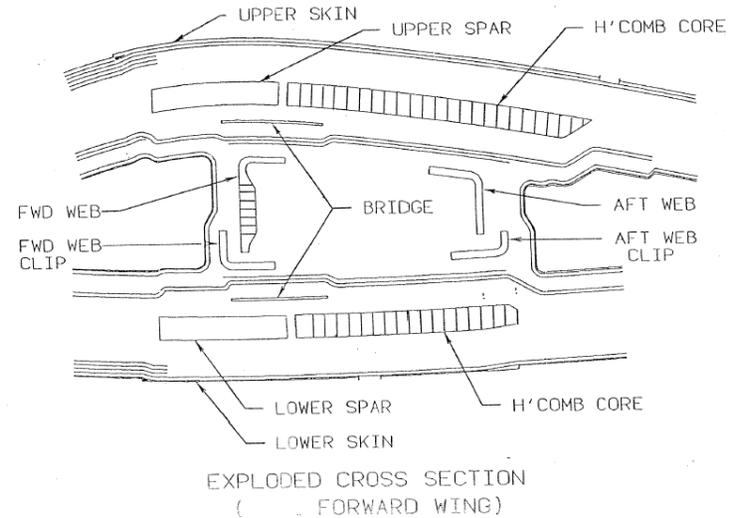
Reduced test matrix
 Factors affecting LEF
 Shared database
Choice of analysis techniques



- Shared database
- Multiple scatter analysis techniques

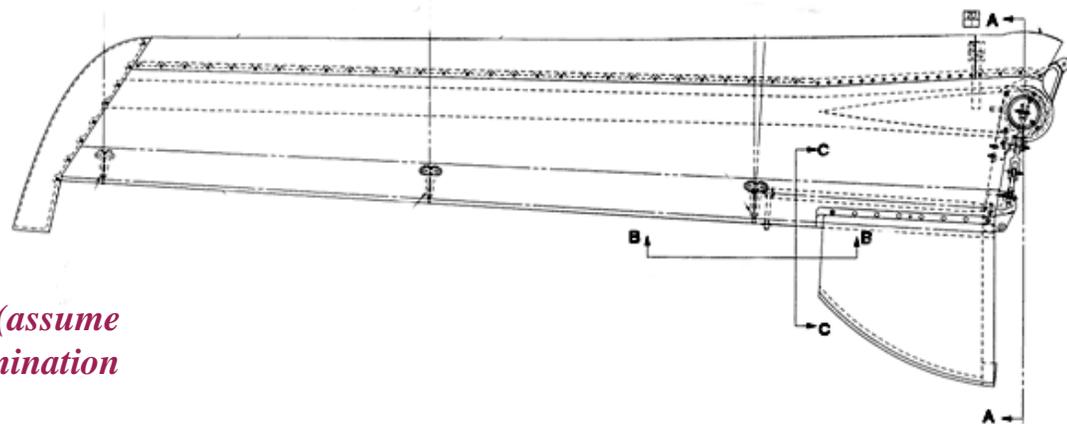
- Improved LEF
- Improved N_F
- Improved “life”
 - Load-life shift





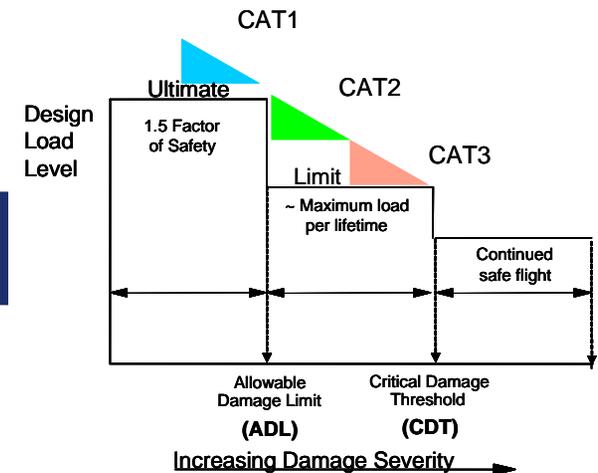
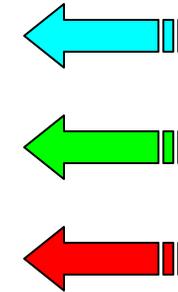
**Beechcraft Starship
 Forward Wings (BSFW)**

Approx. average of 1000 flight hours (assume minimal aging effect), NDE examination



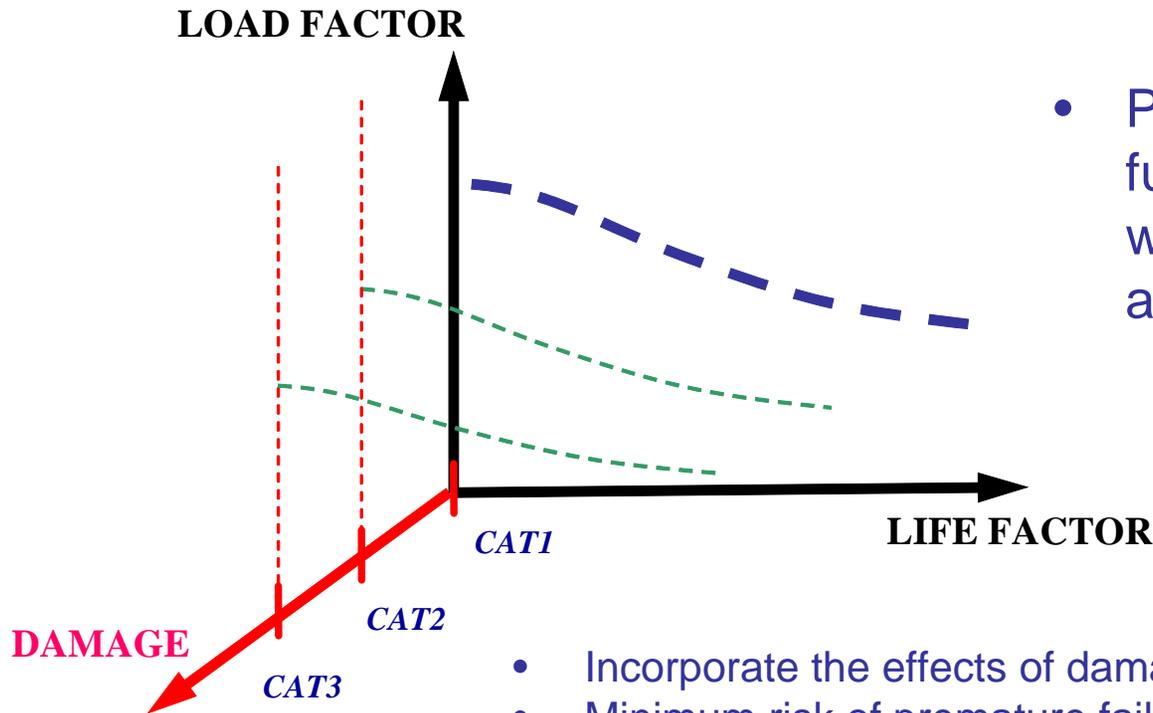
Categories of Damage & Defect Considerations for Primary Composite Aircraft Structures

Category	Examples	Safety Considerations (Substantiation, Management)
<u>Category 1</u> : Damage that may go undetected by field inspection methods (or allowable defects)	BVID, minor environmental degradation, scratches, gouges, allowable mfg. defects	Demonstrate reliable service life Retain Ultimate Load capability Design-driven safety
<u>Category 2</u> : Damage detected by field inspection methods @ specified intervals (repair scenario)	VID (ranging small to large), mfg. defects/mistakes, major environmental degradation	Demonstrate reliable inspection Retain Limit Load capability Design, maintenance, mfg.
<u>Category 3</u> : Obvious damage detected within a few flights by operations focal (repair scenario)	Damage obvious to operations in a “walk-around” inspection or due to loss of form/fit/function	Demonstrate quick detection Retain Limit Load capability Design, maintenance, operations
<u>Category 4</u> : Discrete source damage known by pilot to limit flight maneuvers (repair scenario)	Damage in flight from events that are obvious to pilot (rotor burst, bird-strike, lightning)	Defined discrete-source events Retain “Get Home” capability Design, operations, maintenance
<u>Category 5</u> : Severe damage created by anomalous ground or flight events (repair scenario)	Damage occurring due to rare service events or to an extent beyond that considered in design	Requires new substantiation Requires operations awareness for safety (immediate reporting)



REFERENCE: Ilcewicz, L., “Composite Damage Tolerance and Maintenance Safety Issues,”
FAA Damage Tolerance and Maintenance Workshop, Rosemont, IL, July, 2006.

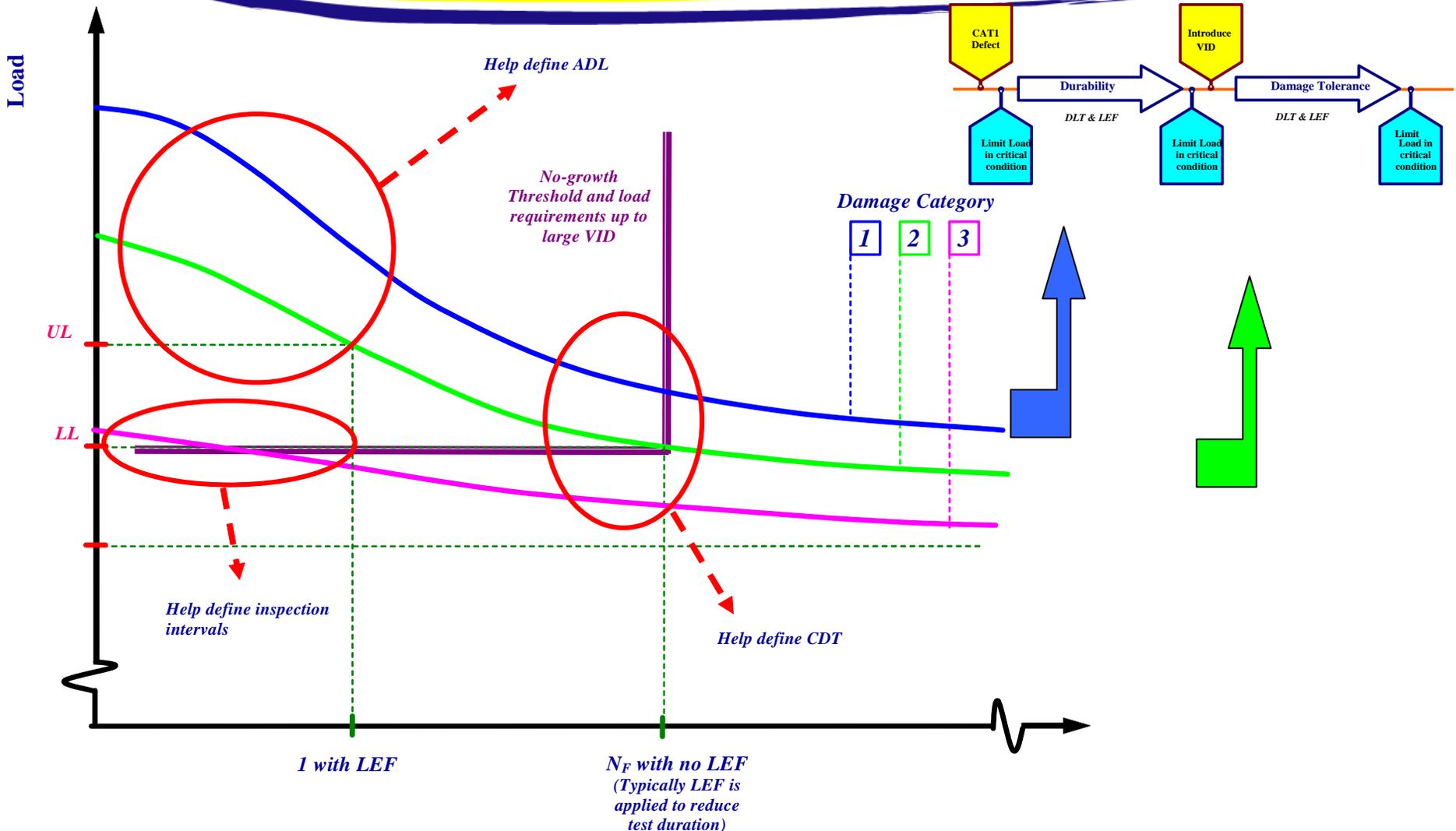
Load-Life-Damage (LLD) Hybrid Approach



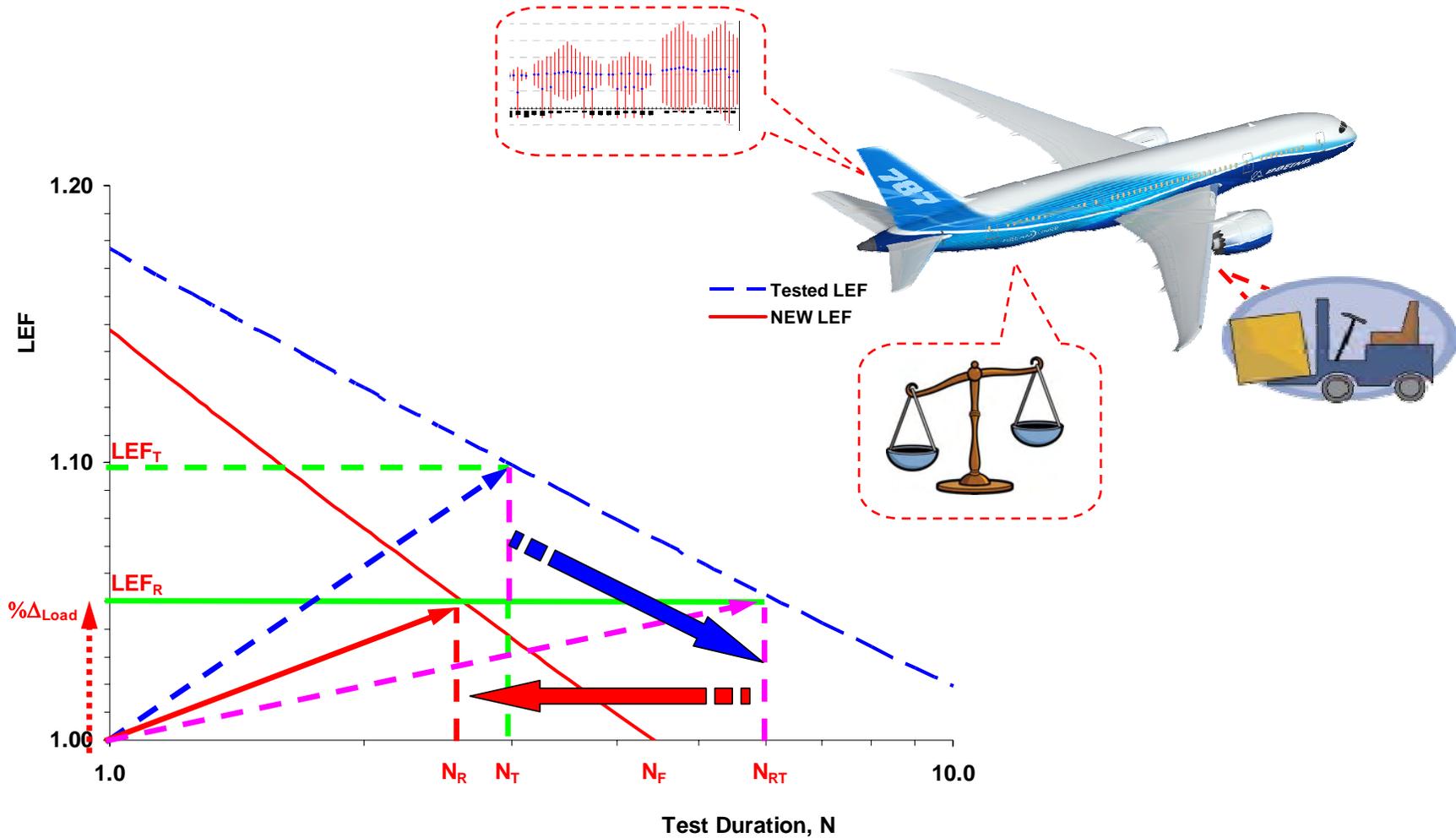
- Provide an opportunity to further investigate large VID without additional test articles

- Incorporate the effects of damage to scatter analysis
- Minimum risk of premature failure of full-scale article
- Application to hybrid structure
- post certification
 - Additional load cases that were not included in the original certification, but found to be significant or worth investigating can be studied

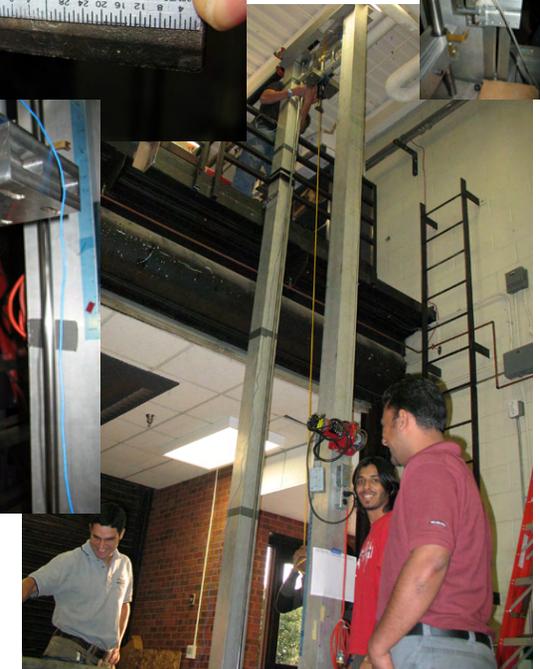
Damage Tolerance Investigation



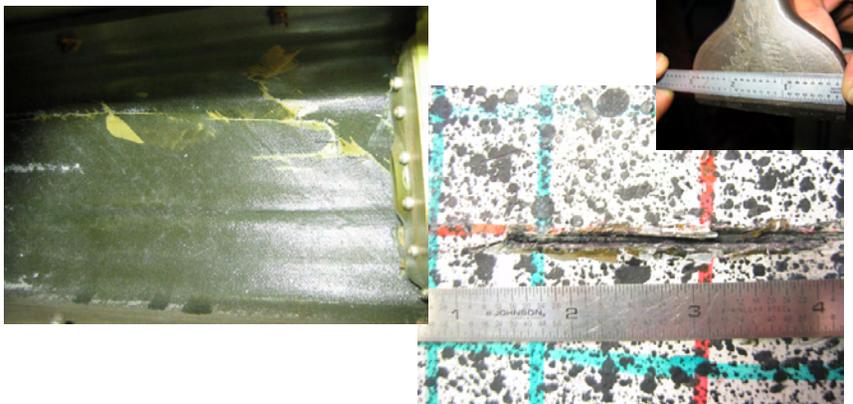
JAMS Design Change Substantiation



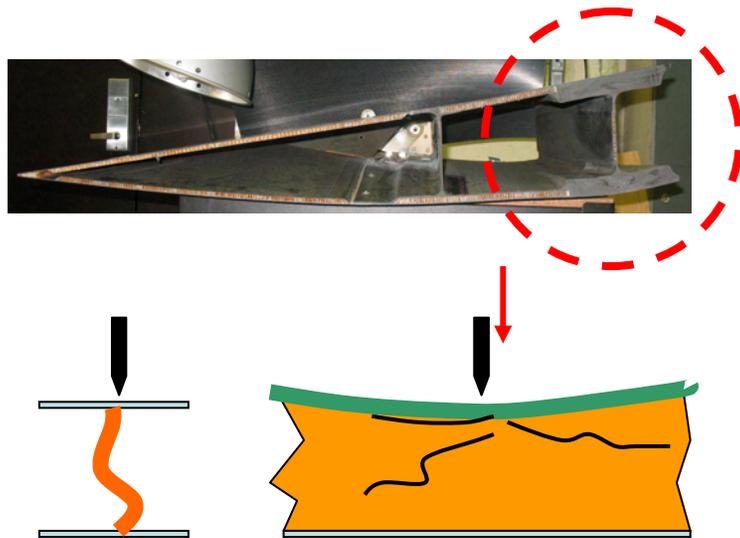
- 1-inch Wedge (pry bar)
- 3-inch Wedge (wood-splitter)



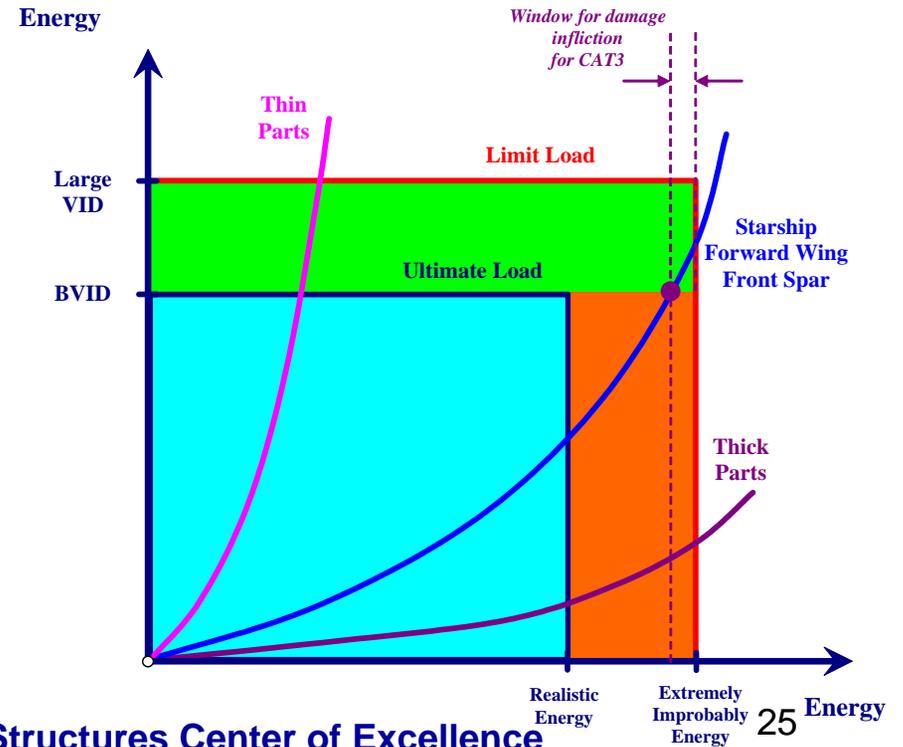
Damage Infliction - BSFW Front Spar -

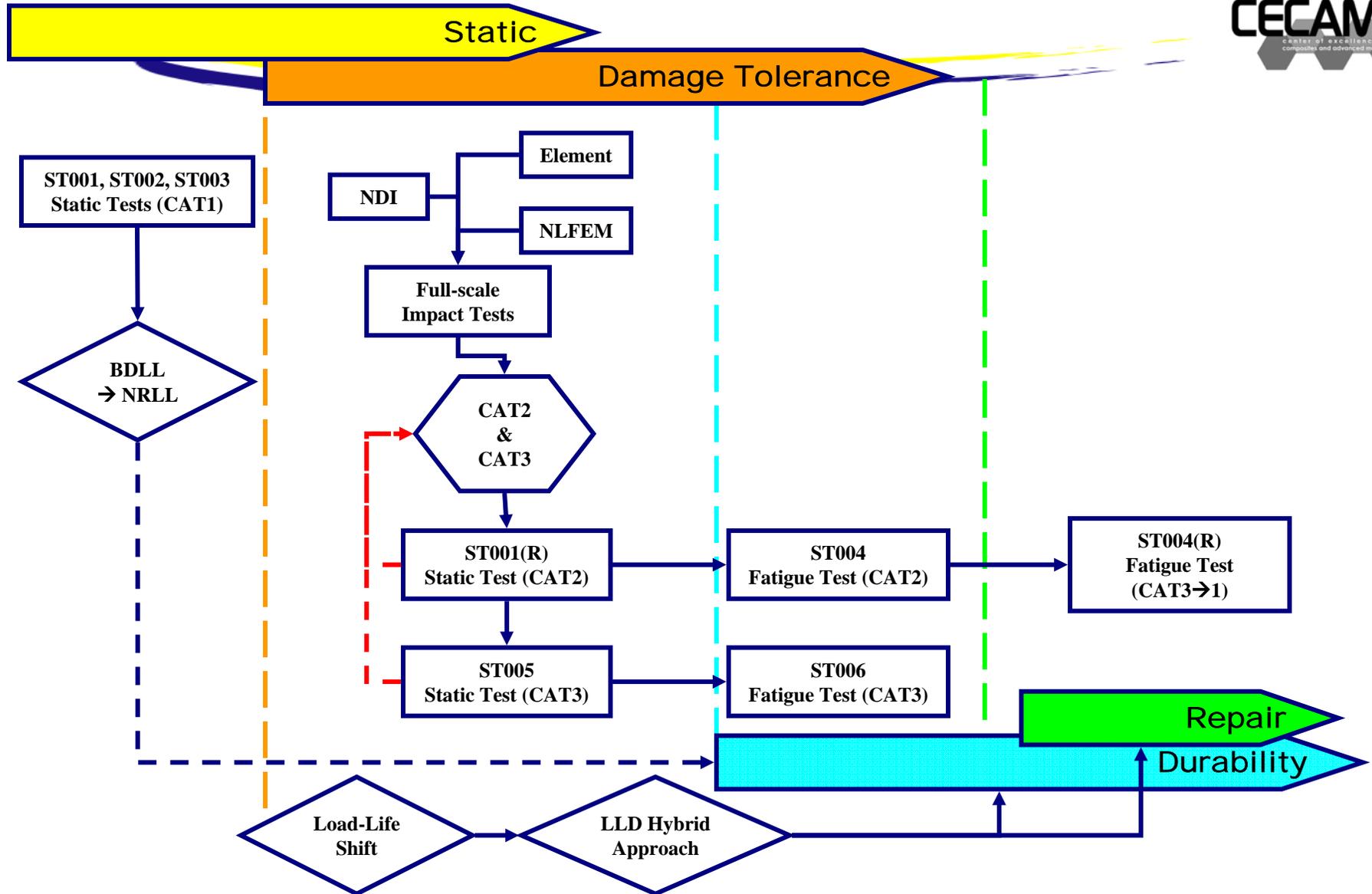


After 1000 ft-lb damage at FWS 66.5 (top skin – front spar)

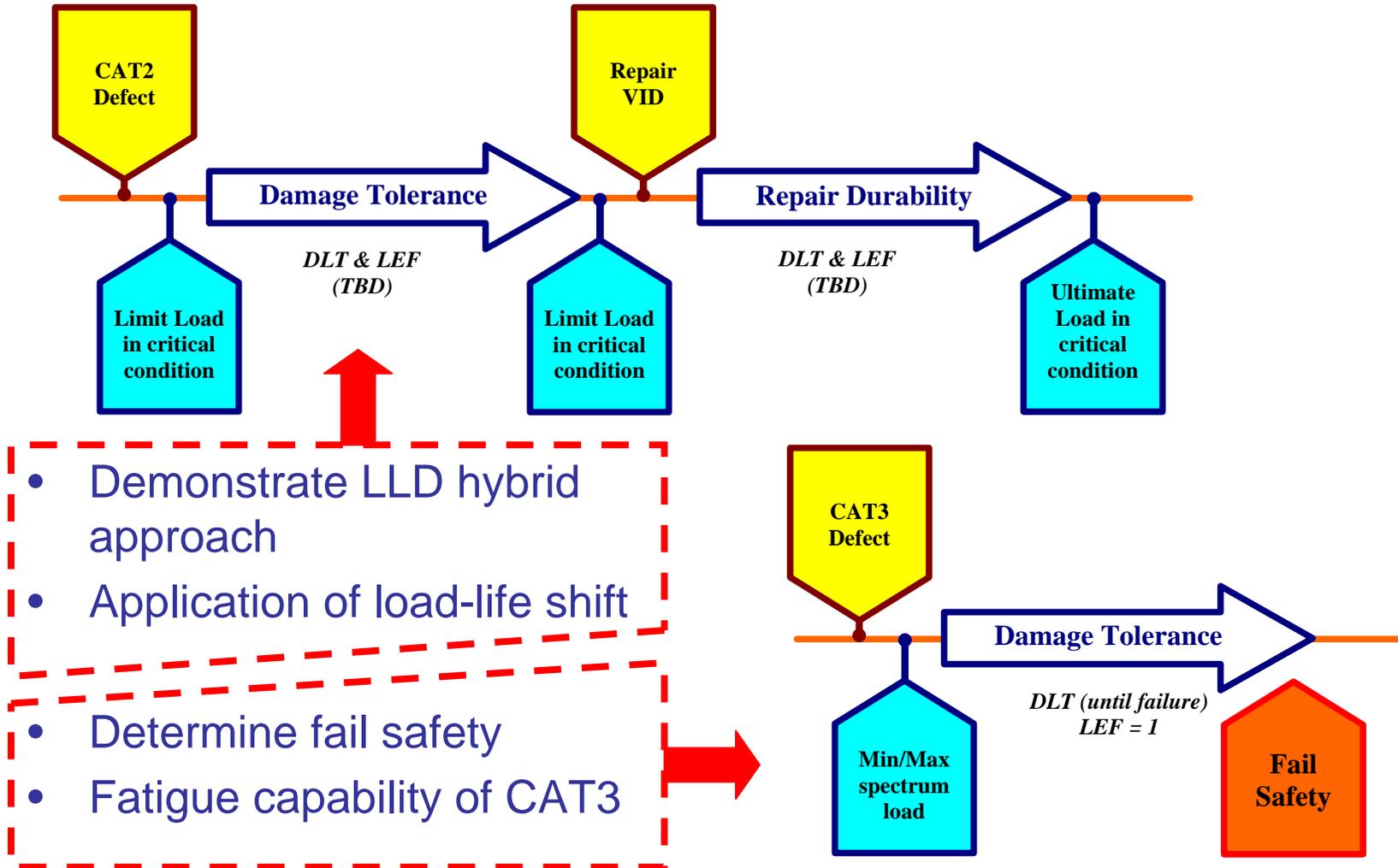


- Primary load path
- Scaling CAT3 damages into full-scale article
- Thick part - unitape
- Wound - no layers

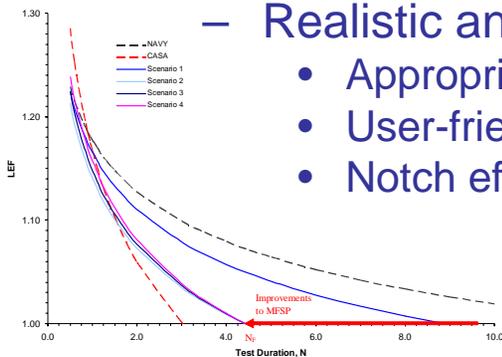
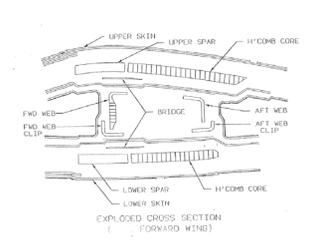




Full-Scale Substantiation - LLD Hybrid Approach -



- FAA guideline document, which demonstrates a “best practice” procedure for full-scale testing protocols for composite airframe structures with examples
 - Cost effective and reliable certification approach(s)
 - Integrate design specific details gained from coupon and subelement tests into the LEF approach
 - Layup, loading modes/R ratios, Environments, ..
 - Bonded joints, interlaminar shear, sandwich, ..
 - Address evolution/maturity of material systems, manufacturing processes, test techniques, etc.
 - Reduced test matrix
 - Shared database concept
 - Realistic analysis approach for scatter
 - Appropriate analysis techniques for diverse design details
 - User-friendly automated procedures and analysis guidelines
 - Notch effects on scatter for damage tolerance testing



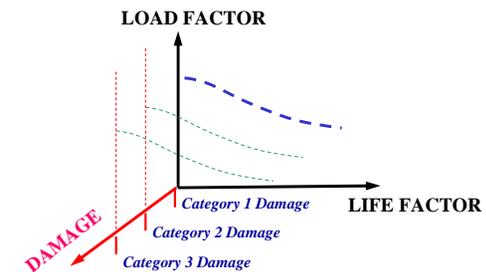
- Incorporation of damage into scatter analysis:
 Load-Life-Damage

- Investigate large VID damage
- Further studies



- Load-Life Shift

- Investigate different categories of damages/repairs in the same full-scale test article damage
- Design changes, i.e. gross weight increase
- LEF during certification vs. improved LEF
 - Reliability of designed life



- Training



- Reliable NDI and health monitoring techniques for damage characterization during full-scale testing and service ~ & Training
- Further studies on extremely improbable high energy impact threats and their impact on the residual strength of the composite structure and inspection intervals

