



Development of Environmental Durability Test Methods for Composite Bonded Joints

Dan Adams, Heather McCartin, Zachary Sievert

University of Utah

JAMS 2018 Technical Review March 23, 2018



FAA Sponsored Project Information

- Principal Investigators:
 - Dr. Dan Adams
- Graduate Student Researchers: Heather McCartin Zach Sievert
- FAA Technical Monitor:
 Ahmet Oztekin
- Collaborators:

Boeing: Kay Blohowiak, Will Grace, Charles Park Air Force Research Laboratory: Jim Mazza 3M Corp: Maha DeSilva



Outline

- Updates:
 - Revision of metal wedge test method (ASTM D3762)
 - ASTM Adhesive Bonding Task Group D14.80.01
- Primary focus: Environmental durability test methods for composite bonded joints
 - Composite wedge test development
 - Comparison of results with other test methods
 - "Smart Wedge" traveling wedge test concept



Background: The Metal Wedge Test

ASTM D3762: "Standard Test Method for Adhesive-Bonded Surface Durability of Aluminum (Wedge Test)"

- Bonded aluminum double cantilever beam loaded by forcing a wedge between adherends
- Assembly placed into test environment (ex: 50^o C, 95% RH)
- Crack growth Δa due to environmental exposure measured following prescribed time
- Able to asses bond quality quickly by causing rapid hydration of oxide layers



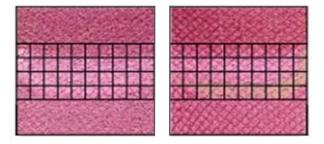


Revision of ASTM D3762: Summary of Proposed Revisions

- Correction of existing errors in standard
- Broadening of scope to include metals other than aluminum as adherends
- Provided additional guidance in specimen manufacturing
- Provided additional detail in test procedure
- Addition of requirement to estimate % cohesion failure in region of environmental crack growth

Percent cohesion failure:

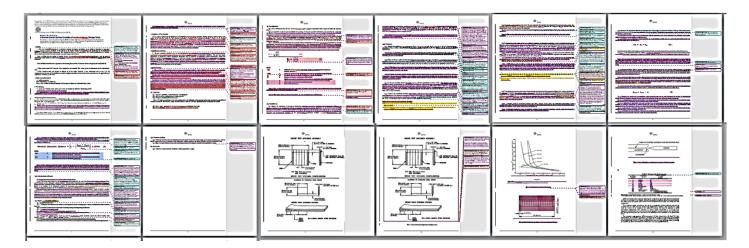
$$\left[1-\left(\frac{A_{nc1}+A_{nc2}}{A_{ext}}\right)\right] x \, 100\%$$





Revision of ASTM D3762: Current Status

- Completed extensive revision of standard
- Initial D14.80 subcommittee balloting
- Addressing remaining concerns from negative votes
- Reballot at concurrent subcommittee/main levels later this summer





Collaborations with ASTM D14 (Adhesives): D14.80.01 Task Group



- Includes ASTM D14 (Adhesives) and ASTM D30 (Composites) members
- Meets concurrently with ASTM D30 to allow for greater participation
- Balloting through D14.80 subcommittee and D14 main
- Technical contact(s) from D30 to attend D14 meetings and provide TG status reports

Current Activities

- ASTM D3762 Metal Wedge Test revision
- ASTM D5656 Thick Adherend Lap Shear Test revision
- Composite Wedge Test development/standardization



Current Activities: ASTM D14.80.01 Task Group

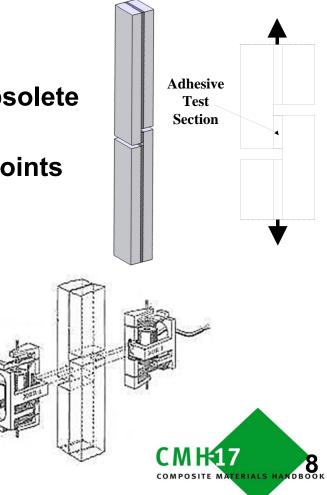


Improvements to ASTM D5656–Thick Adherend Lap Shear Test

- Best practices for shear strain measurement
 - Identify suitable replacement(s) for obsolete
 KGR-1 extensometer
 - Determination of optimal attachment points for shear strain measurement

Round-robin investigation initiated

- Two paste adhesives
- Four adhesive thicknesses
- Three labs/measurement methods
- In conjunction with CMH-17 Testing Working Group



Outline

- Updates:
 - Revision of metal wedge test method (ASTM D3762)
 - ASTM Adhesive Bonding Task Group D14.80.01
- Primary focus: Environmental durability test methods for composite bonded joints
 - Composite wedge test development
 - Comparison of results with other test methods
 - "Smart Wedge" traveling wedge test concept



Overview:

Development of a Composite Wedge Test:

Additional Complexities:

- Variable flexural rigidity (E_f*I) of composite adherends
- Environmental crack growth dependent on adherend flexural rigidity
 - Flexural rigidity must be within an acceptable range or...
 - Must tailor wedge thickness for composite adherends or...
 - Must use another quantity to assess durability





Why Environmental Durability Tests of Composite Bonded Joints?

"There is currently no known mechanism similar to metal-bond hydration for composites"

- Ensure longer-term environmental durability of composite bonds
- Investigate effects of environmental exposure on performance of bonded composite joints
 - Failure mode: cohesion versus adhesion failure
 - Estimate fracture toughness reduction
- Evaluate effectiveness of surface preparation



Use of Fracture Toughness, G_c To Assess Environmental Durability

Consider composite adherends as cantilever beams

- Measured values of crack length, a
- Known value of beam deflection, δ

 $\delta = t/2$ (half of wedge thickness)

Tip deflection of a cantilever beam:

$$T = \frac{E_f b h^3 t}{8 a^3}$$

Strain energy due to bending: $U = \frac{1}{2}T \delta$

Strain energy release rate: $G_c = \frac{dU}{dA}$

$$\Rightarrow G_c = \frac{3E_f t^2 h^3}{16 a^4} \left[\frac{1}{(1+0.64 \frac{h}{a})^4} \right]$$

a δ δ δ δ $\delta = \frac{t}{2} = \frac{P l^3}{3 E_f I} = \frac{T a^3}{3 E_f I}$

- a = crack length
- t = wedge thickness
- h = adherend thickness
- b = specimen width
- T = load to deflect tip of beam
- E_f = flexural modulus
- *G_c* = fracture toughness

12

Correction factor for crack tip rotation

Experimental Investigation: Composite Wedge Test Development

- IM7/8552 carbon/epoxy adherends
- AF163-2K film adhesive
- "Ideal Bond": Grit-blast & acetone wipe bond surfaces
- Multiple adherend thicknesses to produce different flexural rigidities (E_f * I)
 - 13, 15, 17, 19, 21, 23 ply thicknesses
 - (0.10 to 0.17 in thick adherends)
- 122°F (50°C) and 95% humidity environment for 5 days





Effects of Composite Adherend Thickness: Crack Length and Growth Measurements

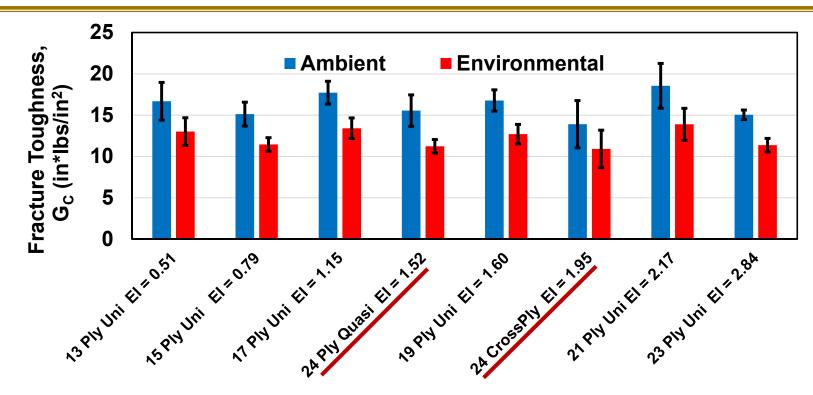
122°F (50°C) and 95% humidity environment 3.5 0.18 Crack Length, a Crack Growth, Δa Change in Crack Length, ∆a (in) 0.16 3 Final Crack Length, a (in) 0.14 2.5 0.12 2 0.10 0.08 1.5 0.06 1 0.04 0.5 0.02 0 0.00 13 ply 15 ply 17 ply 19 ply 21 ply 23 ply 13 ply 15 ply 17 ply 19 ply 21 ply 23 ply (0.094 in) (0.110 in) (0.122 in) (0.138 in) (0.154 in) (0.169 in) (0.138 in) (0.154 in) (0.094 in) (0.110 in) (0.122 in) (0.169 in) **Composite Adherend Thickness Composite Adherend Thickness**

Increasing adherend thickness (and flexural stiffness)...

- Increases crack length, a
 - Increases crack growth, Δa

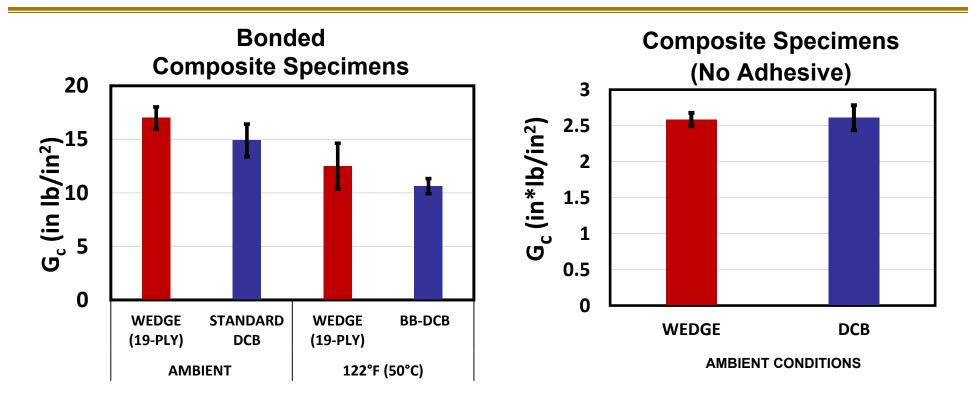


Wedge Testing of Multidirectional Laminates: Fracture Toughness Values



- Apparent facture toughness values remain relatively constant
- Provides estimate of fracture toughness at ambient conditions
- G_c values from quasi-isotropic and crossply laminates consistent with previous unidrectional laminates

Composite Wedge Test Development: Comparisons With DCB Test



General agreement to date between double cantilever beam (DCB) and composite wedge test results Investigating Accuracy of G_c Values From Wedge Test: Determination of Flexural Modulus, E_f

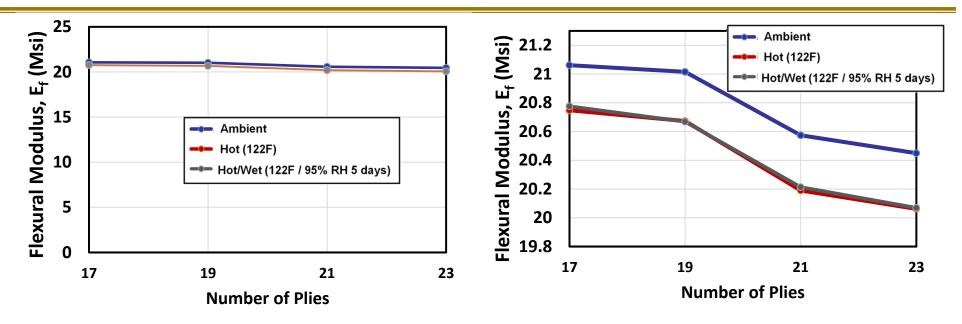
Require value of flexural modulus, E_f, for calculating fracture toughness,

$$G_{c} = \frac{3 E_{f} t^{2} h^{3}}{16 a^{4}} \left[\frac{1}{(1+0.64 \frac{h}{a})^{4}} \right]$$

- E_f value should be representative of that experienced during wedge testing
- What type of test should be used to measure E_f?
- What environment should testing be performed at:
 - How does environmental exposure affect E_f?
 - Can RT/ambient E_f measurement be used?



Three-Point Flexural Modulus (E_f) Testing of Composite Adherends: Effects of Environmental Conditioning



- Three-point flexure testing
- Less than 2% reduction in E_f due to conditioning environment (122 °F, 95% RH for 5 days)
- Flexure testing of adherends at RT/Ambient conditions appears suitable for E_f determination

Since We're Testing Adherends to Measure E_f... Why Not Measure E_f * I ?

G_c written in terms of flexural modulus, *E_f*

$$G_{c} = \frac{3 \, E_{f} \, t^{2} \, h^{3}}{16 \, a^{4}}$$

 G_{c} written in terms of flexural rigidity, E_{f}

$$G_c = \frac{9 \left(\underline{E_f} \, I \right) t^2}{4 b a^4}$$



a = crack length t = wedge thickness h = adherend thickness b = specimen width E_f = flexural modulus I = area moment of inertia

 G_c = fracture toughness

Measuring flexural rigidity $E_f I...$

- Allows for direct slope measurement from load/displacement curve (*P*/δ)
- Eliminates need for adherend thickness measurement
- Possible elimination of correction factor

Use of Effective Flexural Rigidity For Fracture Toughness Determination

Express fracture toughness written in terms of E_f I:

$$G_c = \frac{9(E_f I) t^2}{4b a^4}$$

 Measure *E_f I* directly using post-tested wedge specimen under DCB type loading

$$E_f I = \frac{2a^3}{3} \left(\frac{\Delta P}{\Delta \delta} \right)$$



a = beam span (crack length)

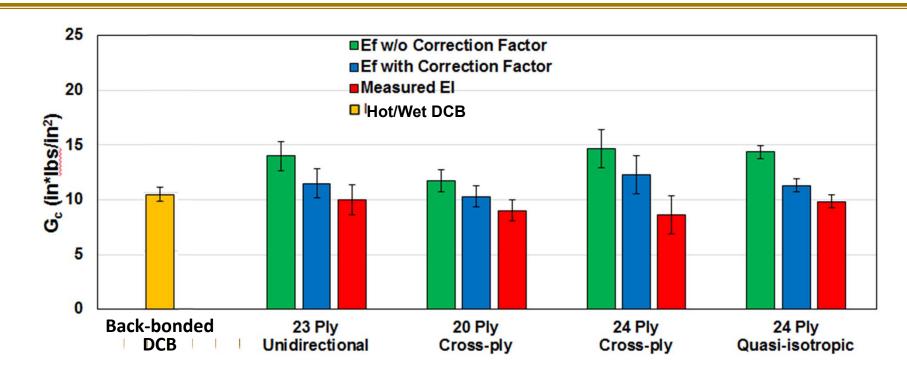
P = applied force

- δ = crosshead displacement
- *t* = wedge thickness
- *E*_f = flexural modulus
- I = moment of inertia



Correction for crack tip rotation
 "built-in" to effective *E_f I* measurement

Comparison of Wedge Test and DCB Test Results: 50°C, 95% RH, 5 days



General agreement with both closed-form correction factor and measured E_f l approaches

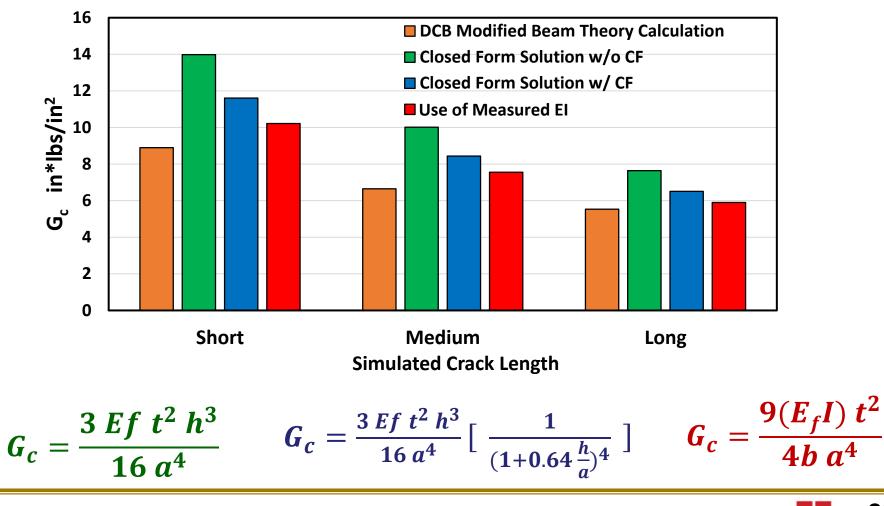


Current Focus:

Numerical Simulation To Investigate Correction Factor

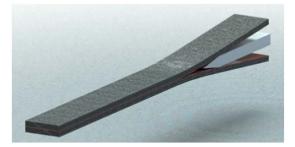
- 3D finite element analysis of composite adherends with adhesive layer
- Prescribed displacement loading simulating wedge
- Simulation of three different crack lengths
- Simulation of three different adhesive thicknesses
- Identification of best suited methodology for apparent G_c determination

Comparison of Methods for G_c **Determination: Preliminary Results From Numerical Simulation**

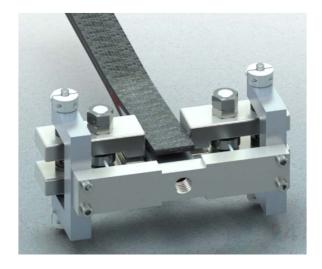


UNIVERSITY OF UTAH What if the Wedge Could Measure Opening Force During Wedge Testing?

- Continuous opening-force measurement as wedge driven through specimen
- Monitor for drop in measured force
 - Increased crack length ahead of wedge
 - Reduced fracture toughness
- Retain wedge in specimen for environmental durability test
- Similar to traveling wedge test, but with force-sensing "smart" wedge

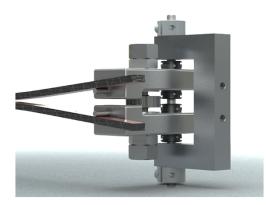


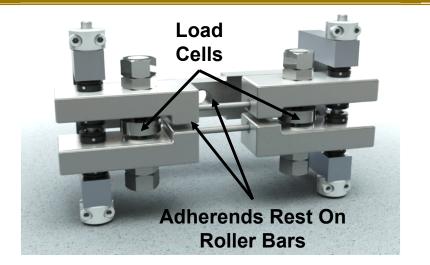




"Smart Wedge" Concept

- Two compression load cells to measure opening force
- Adherends supported by roller bars
- Linear bearings allow for vertical displacement
- Wedge driven through bondline or held in place







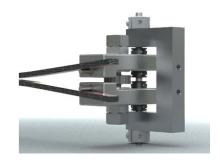
"Smart Wedge" Concept: Fracture Toughness Measurement

- G_c written in terms of E_f I: $G_c = \frac{9(E_f I) t^2}{4 b a^4}$
- From beam theory, solving for crack length, a

$$G_c = \left[\frac{9 P^4 t^2}{4 b^3 (E_f I)}\right]^{1/3}$$

- Can calculate G_c knowing:
 - P (measured force)
 - *t* (wedge thickness)
 - Flexural rigidity, E_f I (measured)

Do not need crack length measurement!



 $|3(E_f I)t|$

3

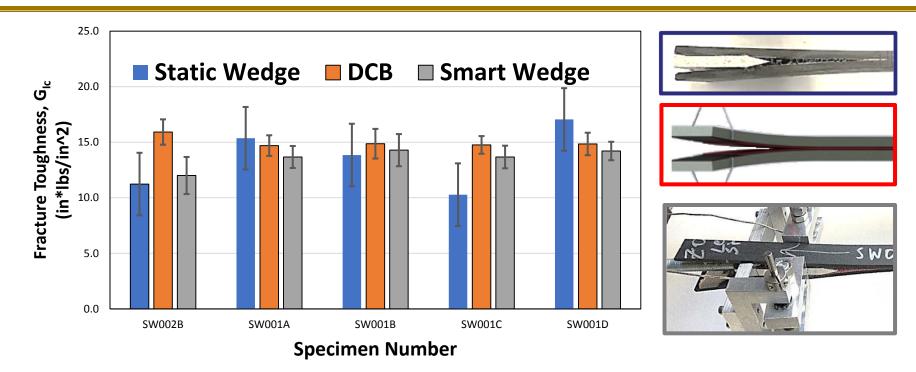
P = applied force

t = wedge thickness *E*_f = flexural modulus

I = moment of inertia

a = beam span (crack length)

Preliminary Results: "Smart Wedge" Testing

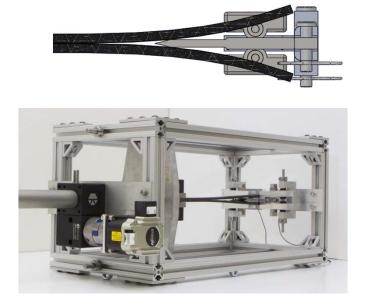


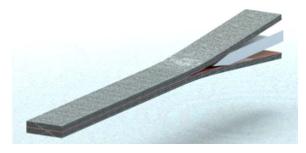
- 3 tests (DCB, static wedge and Smart Wedge) performed on each bonded composite specimen
- Initial results appear promising



Smart Wedge Testing: Envisioned "Hybrid" Procedure

- Install specimen into smart wedge, retract installation wedge
- Obtain initial load and crack length measurements, calculate flexural rigidity, E_f I
- Perform "traveling wedge" type testing, obtain real-time fracture toughness G_c estimates
- Halt traveling wedge, reinsert wedge, and subject to environmental exposure for durability assessment





Plans for Upcoming Research: Development of Environmental Durability Test Methods for Composite Bonded Joints

- Establish limits of applicability and recommended procedures for the composite wedge test
 - Acceptable range of flexural rigidities E_f I
 - Method of G_c determination
- Assessment of "Smart Wedge concept for hybrid assessment of bond quality over larger bond areas
 - Continuous fracture toughness
 measurements
 - Environmental durability assessment when desired







BENEFITS TO AVIATION

- Improved environmental durability test method for metal bonds (metal wedge test, ASTM D3762)
- Composite wedge test for assessing the environmental durability of composite bonds and assessing surface preparations
- Hybrid traveling wedge/static wedge test for evaluation of larger bond areas
- Dissemination of research results through FAA technical reports and conference/journal publications



Thank you for your attention!

Questions?

